(MASA-CR-171830) IMPECVED CHEITER WASTE

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MCDONNELL DOUGLAS ASTRONAUTICS COMPANY

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CORPORATION

DOUGLAS

IMPROVED ORBITER WASTE **COLLECTION SYSTEM STUDY**

Final Report

NOVEMBER 16, 1984

MDC H1360

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CONTRACT NASA 9-17181

DRL: T-1837, LINE ITEM 1

DRD: MA-183TH

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FINAL REPORT IMPROVED ORBITER WASTE COLLECTION

SYSTEM STUDY

1.0 ABSTRACT

This report is the result of a three month study under NASA contract NAS 9-17181 to develop design concepts for improved fecal waste collection both on the Space Shuttle Orbiter and as a precursor for Space Station. The Study was initiated to resolve the inflight usage problems associated with the existing Orbiter waste collection subsystem and to provide a basis for the selection of an optimum waste collection system concept which may utlimately result in the development of an Orbiter flight test article for concept verification and subsequent production of new flight hardware.

Two concepts have been selected for Orbiter and are shown in detail in Section 6.0. Task

4. Additionally, Section 6.0, Appendix A contains one concept selected for application
to Space Station. The contractually required Systems Requirements Definition Document
and a packet of layouts are included as appendices under separate covers.

This document constitutes completion of the final task in the study.

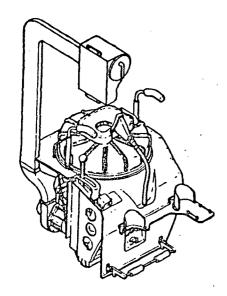
2.0 RESULTS

The study culminated in the selection of two concepts which are feasible for installation into the Orbiter. The first concept is a repackaged Skylab waste collection system (NCS) requiring very little development. The second concept is a centrifugal compaction device which requires additional development but is retrofittable directly into the existing Orbiter commode structure. A third system, the closed loop macerator, is suggested as a Space Station NCS as it has no venting requirements (see Figure 1). These concepts are discussed in detail in the text of Section 6. The data is in the format of the Design Concept Presentation given at Johnson Space Center on November 2, 1984.

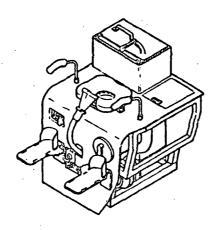
The Design Concept Presentation is organized as shown below. Note the addition of Appendices D and E which are under separate cover.



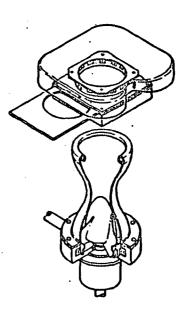
SELECTED CONCEPTS



CENTRIFUGAL COMPACTION CONCEPT



1-G SKYLAB
CONFIGURATION



CLOSED LOOP MACERATOR
CONCEPT

FIGURE 1

Organization of Design Concept Presentation (Section 6.0):

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Background	1
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Appendix B Other Semi-Final Concepts	96
Appendix C Skylab System Data	120
Appendix D System Requirements Definition Document	
Appendix E Layouts of WCS Design Concepts	

3.0 CONCLUSIONS

The 1-G Skylab Configuration and Centrifugal Compaction Concept Waste Collection Systems have been defined as optimal choices for retrofit into the Shuttle Orbiter. The first concept has the advantages of being a simple, proven system with minimal risk and low development. The need for fecal bag handling is present, but bag sealing and handling

methods have been significantly improved over the original Skylab system. Similarly, the Centrifugal Compaction Concept utilizes a collection method similar to that of the existing Shuttle system while adding the ability to compact waste to increase storage capacity. Additionally, this concept utilizes the existing commode structure and plumbing network, making it easier to retrofit into the Orbiter. Key features of both concepts include their use of existing Orbiter commode flight hardware when possible and the capability to perform in-vehicle turnaround.

4.0 RECOMMENDATIONS

Implementation of follow-on tasks such as additional study, preliminary design, development of specific concepts, or test hardware procurement are options recommended to NASA.

5.0 APPLICABLE DOCUMENTS

The documents applicable to the Improved Orbiter Waste Collection System Study are given below.

5.1 NASA Documents

Shuttle Flight Operations Manual, Vol. 12 - Crew Systems, Basic PCN-6, JSC, November 15, 1983

WCS 2102B Waste Collection System Workbook, JSC, March 2,

1984

TM X-64814 MSFC Skylab Mission Report - Saturn Workshop,
October, 1974

MSC-01549 Skylab Program Operational Data Book, Vol. IV,
Skylab-I Performance Data, Revision A, JSC,
October 1972
Improved Waste Collection System Initial Review

[Handout], JSC, July 20, 1984

5.2 MDAC Documents

1B87234-1 Separator, Centrifugal Urine, February 2, 1971

5.3 Rockwell International Documents

MC282-0069 Waste Collection Subsystem Procurement Document,
January 24, 1984

5.4 General Electric Documents

47J232750 WCS Assembly [Drawing], October 5, 1982

6.0 DESIGN CONCEPT PRESENTATION MATERIAL

The following text contains material from the November 2, 1984

Design Concept Presentation at Johnson Space Center.



IMPROVED ORBITER WASTE COLLECTION SYSTEM DESIGN CONCEPT PRESENTATION JSC

2 NOVEMBER 1984



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Background

Task 1 Review

Task 2 Design Studies

Task 3 Selection Process

Task 4 Design Concept Presentation

Task 5 Review Requirements

Task 6 Document Requirements

Appendix A Space Station WCS Concept

Appendix B Other Semi-Final Concepts

Appendix C Skylab System Data



BACKGROUND



CHRONOLOGY OF EVENTS

Initial Contact by JSC

RFP

Study Proposal Submitted

ATP

JSC Initial Review

Midterm Review

Formal Presentation

Final Report Due

March 30, 1984

May, 1984

July 6, 1984

July 20, 1984

September 27, 1984

November 2, 1984

November 16, 1984

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TASK 1 ORBITER WASTE COLLECTION SYSTEM INITIAL REVIEW

- **Overview of Existing Shuttle WCS**
- **Subsystem Operating History**
- **B** Identification of Development Needs



TASK 1 ORBITER WASTE COLLECTION SYSTEM INITIAL REVIEW 20 JULY 1984

VEC903

Summary of Inflight Problems to Resolve in Improved Waste Collection System

- Generation of Fecal Dust/Particulate Matter
- **■** Odor
- Paper Storage Separate From Feces
- Lack of Compaction Capability
- Corrosion
- **Buildup of Urine Solids**
- Noise
- **Lengthy Turnaround Time**
- Component Failures
- **B** Excessive Crew Involvement and Cleanup

MCDONNELL DOUGLAS

- Analytical Studies
- Sketches and Layouts



REQUIREMENTS

GENERAL REQUIREMENTS

- O EFFECTIVELY AND HYGIENICALLY SEPARATE WASTES FROM THE CREWMEMBER
- O STORE THE WASTES IN A SAFE, ODORLESS FORM SEPARATE FROM THE CREW COMPARTMENT

SPECIFIC REQUIREMENTS

- O ACCOMMODATE USE BY BOTH MALES AND FEMALES
- O URINE COLLECTION INTERFACE SHOULD BE INDIVIDUAL
- O BE STRAIGHT-FORWARD AND SIMPLE IN USE AND NOT TAKE EXCESSIVE TIME
- O CAPACITY SHOULD NOT BE LIMITED BY PAPER; I.E., SEPARATE PAPER COMPARTMENT OR COMPACTION FOR PAPERS AND/OR FECES.
- O REQUIRE ONLY MINIMAL TRAINING FOR SUCCESSFUL CREW USE
- O PROVIDE NO HANDLING OF WASTES BY THE CREW
- O PROVIDE PROPER STOOL SEPARATION DURING USE
- O PROVIDE ADEQUATE BODY STABILIZATION FOR USE
- O PROVIDE POSITIVE COLLECTION AND RETENTION OF WASTES AND PAPER FOR A MINIMUM OF 210 MAN-DAYS OF USE
- O INCLUDE PROVISIONS FOR BACTERIA AND ODOR CONTROL
- O BE QUIET DURING OPERATION; NOT DISTURB SLEEP (GOAL: NOISE CRITERIA (NC) 40)
- O BE MAINTAINABLE AT THE LAUNCH SITE; REQUIRE MINIMAL TURNAROUND TIME/IMPACTS (GOAL: IN-VEHICLE GROUND MAINTENANCE)
- O MINIMIZE EXPENDABLES, WEIGHT, POWER, AND VOLUME WITHOUT COMPROMISING SUBSYSTEM OPERATIONAL CHARACTERISTICS
- O BE RELIABLE AND SHOULD INCUDE REDUNDANT ELECTRICAL COMPONENTS AND DUAL SEALS WHERE PRACTICAL
- O BE RETROFITTABLE WITHIN CURRENT SYSTEM COMPARTMENT INTO THE ORBITER FLEET IN THE FIELD, I.E., KSC

VEC905

CRITICAL DESIGN/TRADEOFF PARAMETERS

- m Feces Separation, Collection, and Containment
- **B** Paper Disposal
- **Ease of Operation**
- **Body Stabilization**
- **M** Noise
- Maintainability
- **Meight**
- **Power**
- Retrofittability
- Design Risk
- **■** Cost

MCDONNELL DOUGLAS



TASK 3 DESIGN CONCEPT SELECTION

VEC906

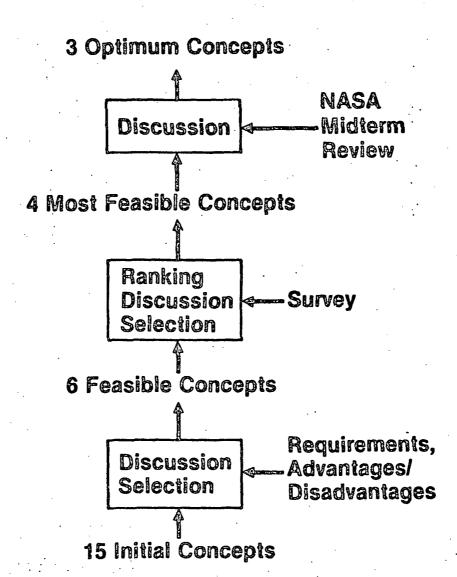


- Evaluate Concepts With Respect to Waste Collection Subsystem Requirements
- Ranking of Concepts in Order of Desirability
- **■** Selection of an Optimum Concept

SELECTION PROCESS



0.3



WCS SURVEY RESULTS

VEC908

Rank	Score			
1	6			
2	5			
3	4	Sample	Size:	10
4	3	•		
5	2			
6	· 1			

Concept	Avg Score	Std Day		
Centrifugal Compaction	4.2	1.4		
Closed Loop Macerator	4.0	2.4		
Skylab Repackaged	3.9	1.4		
Modified Skylab	3.3	0.9		
MDTSCO Trash Ejector	2.9	2.5		
1 Week Wall Mount	2.7	0.8		

Respondents: 1. Snyder

- 2. Bastin
- 3. Hofbauer
- 4. Gallo
- 5. Secord
- 6. Kelly
- 7. A-MDTSCO
- 8. B-MDTSCO
- 9. C-MDTSCO
- 10. D-MDTSCO

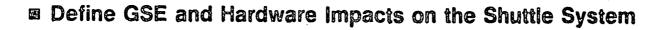


TASK 4 DESIGN CONCEPT PRESENTATION

VEC909



- **B** Summary of Candidate Concepts
- Rationale and Analyses Leading to Selection of the Optimum Concept
- Provide NASA With a Total Understanding of the Selected Concept



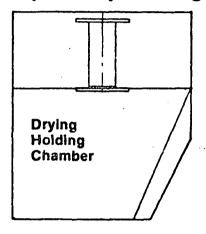


CANDIDATE CONCEPTS



PRELIMINARY WCS CONCEPTS

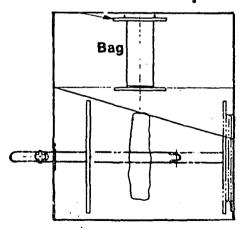
Simple Drop Through



Eliminated Due To .

- Large Volume High Air Loss
- **Inefficient Packing**

Push-Pull Compactor

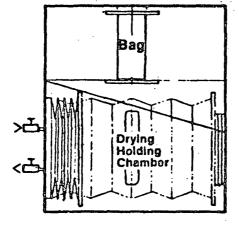


- Large Volume High Air Loss
- Active Sliding Seals
- **Handle Protrudes Into Crew Compartment**





Bellows Compactor

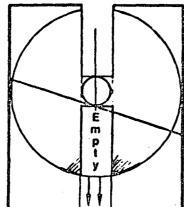


Eliminated Due To . .

- E Large Volume High Air Loss
- **Bag Hang-Up**
- **Bellows Decreases Usable Volume**

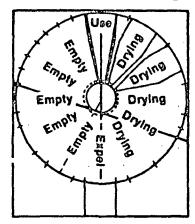


Two Station Rotating Wheel

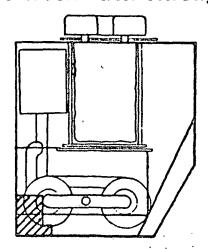


- **Inefficient Use of Volume**
- m No Area for Stowage
- **B** Active Sliding Seals

12/24 Station Rotating Wheel



One Week Push Through



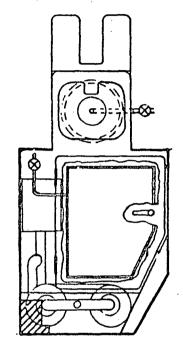
- Eliminated Due To . .
- M No Area For Stowage
- **M** Active Sliding Seals
- **©** Complexity

- Inadequate Stowage Volume
- **B** Psychologically Undesirable





One Week Wall Mount

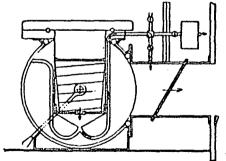


Eliminated Due To . . .

- Poor Psychological Acceptance
- **Weight**
- Marginal Stowage Volume



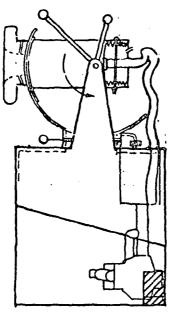
Trash Ejector



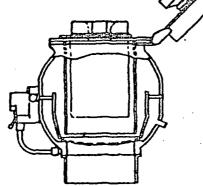
- Mechanical Complexity
- **E Active Sliding Seals**
- a Weight
- No Area For Stowage



Modified Trash Ejector



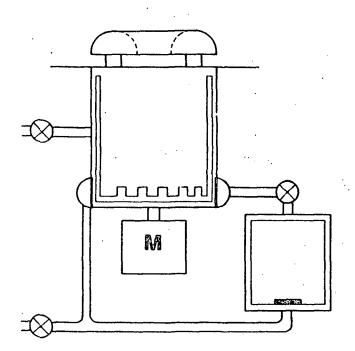
Trash Airlock



Eliminated Due To

- **E** Active Sliding Seals
- Mechanical Complexity
- M Inefficient Packing
- **Weight**
- Mechanical Complexity
- M No Area For Storage





Disposer/Shredder/Grinder

Eliminated Due To . . .

- Mechanical Complexity
- Questionable Feasibility



MOST FEASIBLE CONCEPTS

- 1. Skylab Repackaged Configuration
 - A Repackaged Version of the Proven Skylab Collection System With a Re-configured Processor
- 2. Modified Skylab Concept

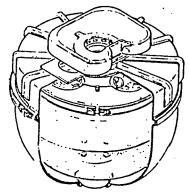
A "Large Bag" Concept (Similar to Skylab) With Significantly Reduced Crew Handling, Weight, and Air Loss

3. Centrifugal Compaction Concept

An Air Entrainment System Featuring Compaction of Paper and Wastes in a Rotating Chamber

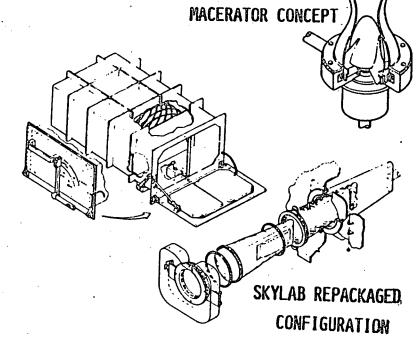
4. Closed Loop Macerator Concept

A Recirculating Fluid System Which Creates a Filterable Slurry of Waste and Water Soluble Biocide

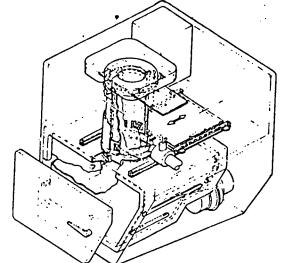


MOST FEASIBLE CONCEPTS

CENTRIFUGAL COMPACTION CONCEPT



CLOSED LOOP

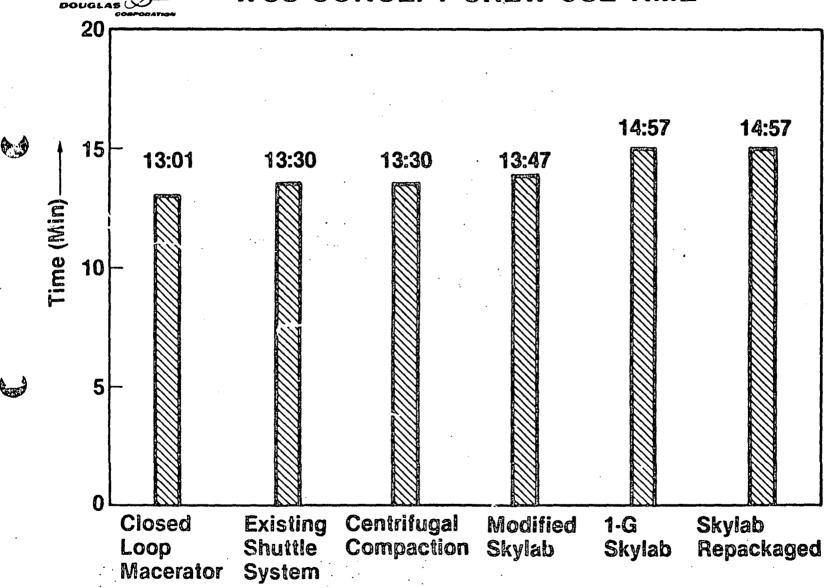


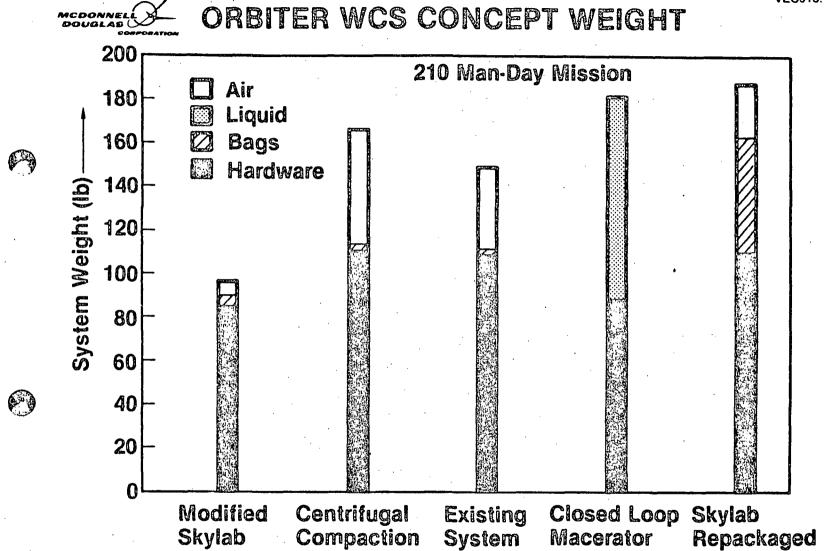
MODIFIED SKYLAB CONCEPT













EXISTING SHUTTLE WCS SYSTEM Estimated Weight Breakdown

VEC916

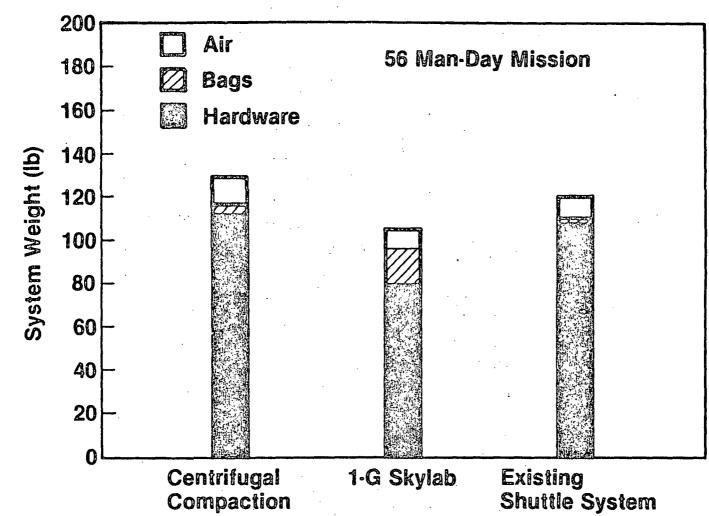
b)
•
•
lb

Note: Current System Omits Motor and Slinger Apparatus

Air Loss: 210 Uses \times 2.4 ft³ \times .0752 lb = 37.9 lb Use ft³



ORBITER WCS CONCEPT WEIGHT





SELECTION OF OPTIMUM WCS CONCEPTS BASED ON

VFC917

- Practicality
- Proven Capability
- Ease of Retrofittability into Orbiter Structure and Interfaces
- Use of Existing Concepts and Flight Qualified Hardware
- **In-Vehicle Maintenance**
- Psychological Acceptability



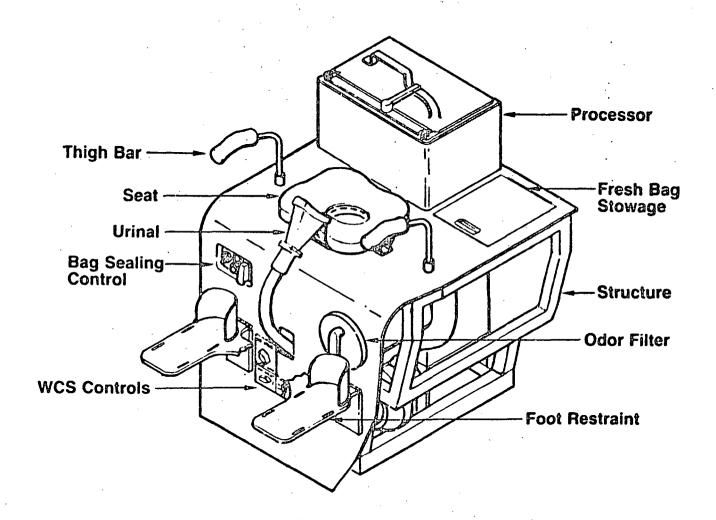
SELECTED CONCEPTS



1-G SKYLAB CONFIGURATION

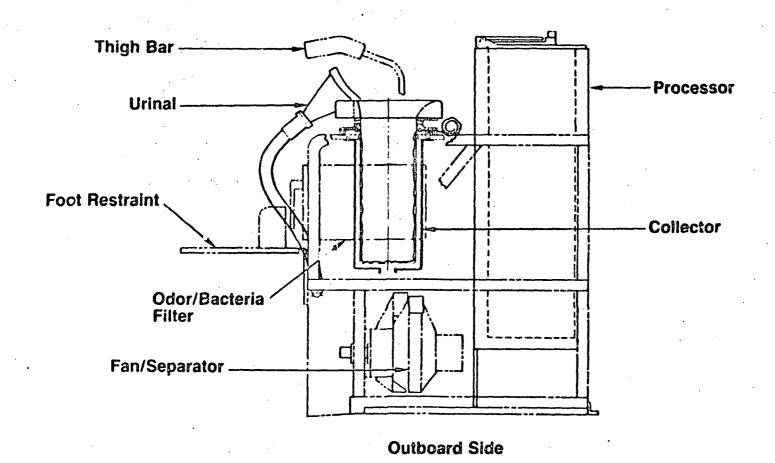


1-G SKYLAB CONFIGURATION





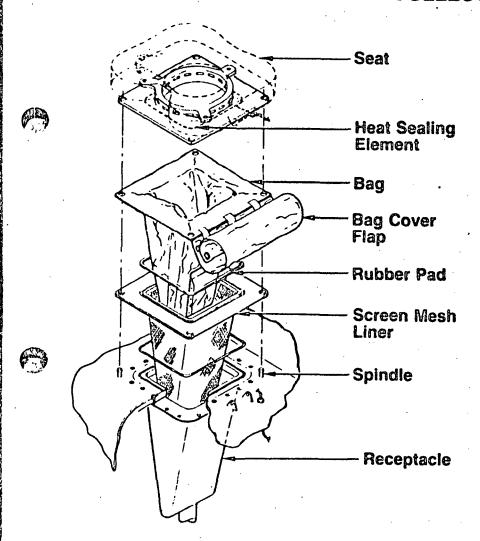
1-G SKYLAB CONFIGURATION

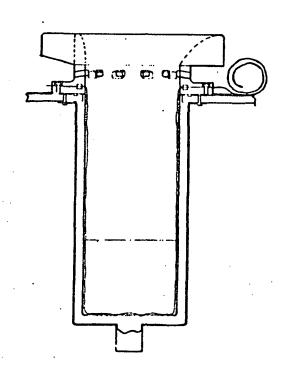


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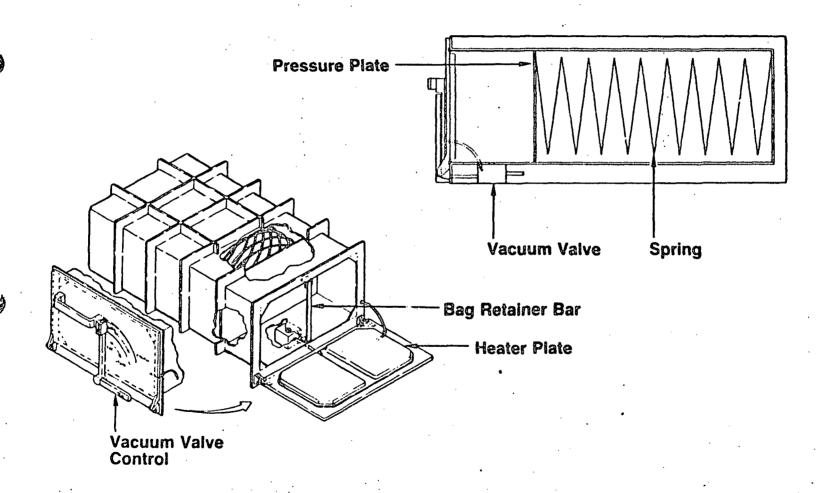
1-G SKYLAB CONFIGURATION COLLECTOR



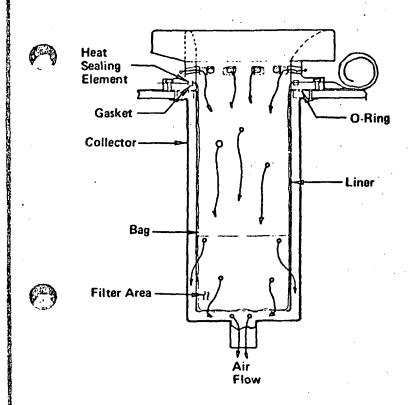




1-G SKYLAB CONFIGURATION PROCESSOR



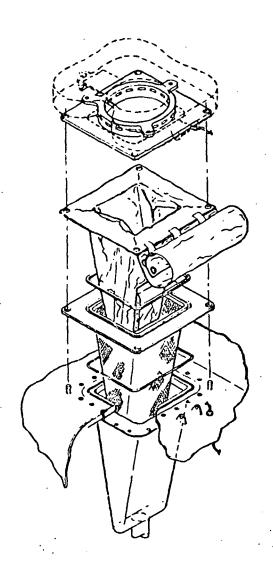
1-G SKYLAB CONFIGURATION COLLECTION



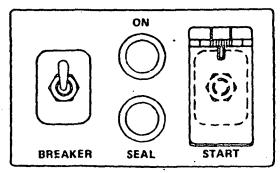
- Bolus Entrained by Airflow From Holes Around Base of Seat
- Air Passes Through Hydrophobic Filter,Mesh Liner and Out of Receptacle



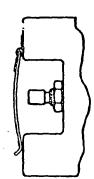
1-G SKYLAB CONFIGURATION BAG SEALING



- Seat Hinged Up
- Bag Cover Flap Secured On Spindles
- **B** Seat Down and Latched
- Push Start Button, Allow Cycle to Finish
- Seat Hinged Up
- Remove Sealed Bag From Spindles

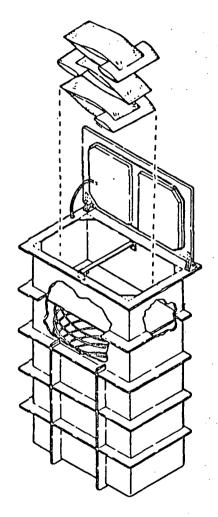




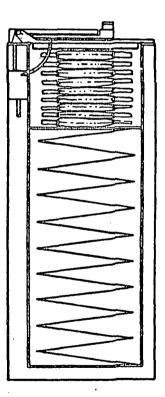




1-G SKYLAB CONFIGURATION BAG STOWAGE

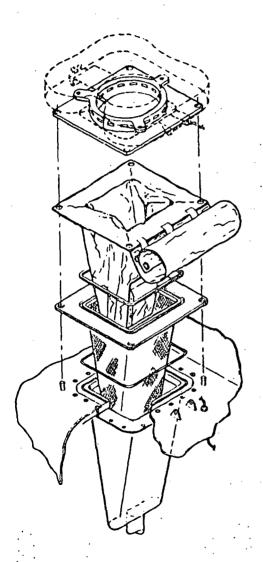


- Sealed Bag Is Folded at Creases
- **□** Processor Vacuum Valve to Cabin
- Open Processor Door
- Release Bag Retaining Bar
- Insert Bag
- Replace Retaining Bar
- **™** Close Processor Door
- **Processor Vacuum Valve to Vacuum**





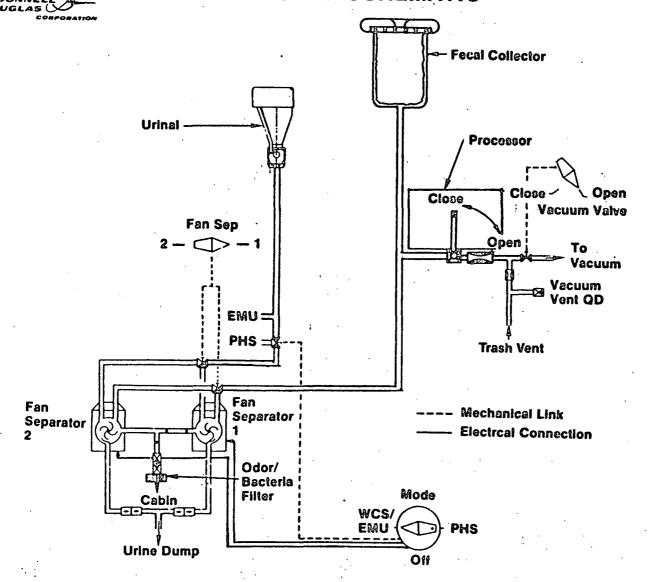
1-G SKYLAB CONFIGURATION BAG INSTALLATION



- **■** Unfold Bag
- Place Bag in Receptacle
- Secure Four Corners on Spindles
- Hinge Seat Down and Latch

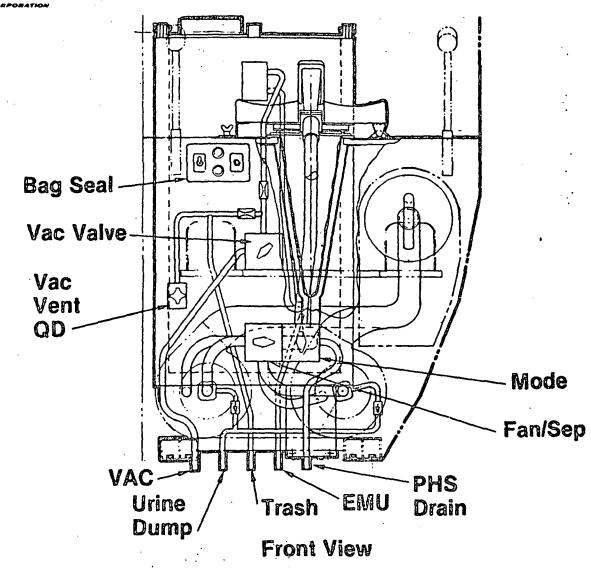
1-G SKYLAB CONFIGURATION SYSTEM SCHEMATIC

VEC849



1-G SKYLAB CONFIGURATION DUCTING AND INTERFACES

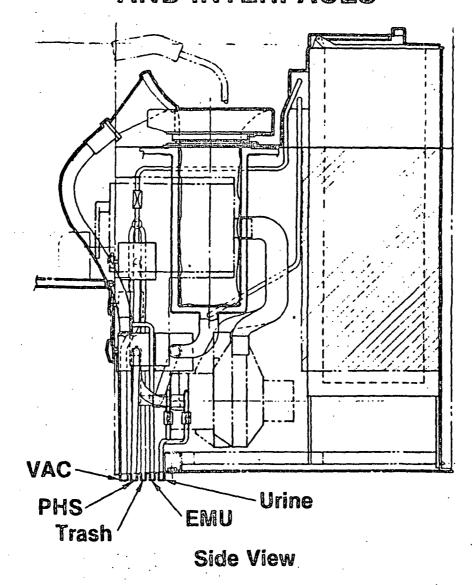
VEC918



20

1-G SKYLAB CONFIGURATION DUCTING AND INTERFACES

VEC919





1-G SKYLAB CONFIGURATION CREW PROCEDURES

		•	CREW	TIME	
			Min.	Sec.	
1.	TURN MODE SWITCH TO WCS/EMU*		•	2	
2.	POSITION BODY AND RESTRAINT SYSTEM			30	
3.	PERFORM DEFECATION AND CLEANUP	. -	12	. 0	•
4.	REMOVE RESTRAINT SYSTEM	. •		15	
5.	UNLATCH AND LIFT SEAT			10	•
6.	SEAL BAG			15	
7.	VERIFY OR CLOSE PROCESSOR VACUUM VALV	Ε,			
	WAIT FOR REPRESSURIZATION			5	
8.	OPEN PROCESSOR DOOR			5	
9.	REMOVE BAG FROM COLLECTOR			5	
10.	PLACE BAG INTO PROCESSOR			15	
11.	CLOSE PROCESSOR DOOR	•		5	•
12.	OPEN PROCESSOR VACUUM VALVE			3	
13.	DISINFECT SEAT			30	
14.	OPEN CLEAN BAG DISPENSER			5	
15.	INSTALL CLEAN BAG			15	
16.	CLOSE CLEAN BAG DISPENSER	•		5	
17.	LOWER SEAT & LATCH			10	
18.	TURN MODE SWITCH TO OFF			2	
	Total	time	14 Min	. 57	Sec.

*FOR URINATION ONLY (AFTER STEP 1), PERFORM URINATION AND CLEANUP AND GO TO STEP 18.



1-G SKYLAB CONFIGURATION GROUND TURNAROUND

		TIME (HK.)
1.	MOVE PROCESSOR VALVE TO CABIN POSITION	
2.	OPEN PROCESSOR DOOR	
3	REMOVE BAGS, PLACE INTO AIR-TIGHT TRANSPORT CONTAINER	.5
4.	REMOVE SPENT ODOR/BACTERIA FILTER	
5.	PLACE FILTER IN TRANSPORT CONTAINER	
6.	REMOVE TRANSPORT CONTAINER FROM ORBITER	
7.	CLEAN & DISINFECT INTERIOR OF COLLECTOR,	71.0
	PROCESSOR AND URINE SYSTEM	ليا
8 ,	CLEAN & DISINFECT EXTERIOR OF WCS	.5
9.	INSTALL FRESH BAG	Ť
10.	INSTALL FRESH ODOR/BACTERIA FILTER	.5
11.	RETURN SYSTEM TO INITIAL CONDITION CONFIGURATION	
12.	VERIFY OPERATION OF SYSTEM	.5
13.	MOVE TRANSPORT CONTAINER TO SERVICE AREA	7
14.	REMOVE WASTE FROM TRANSPORT CONTAINER	1.0
15.	CLEAN AND STORE TRANSPORT CONTAINER	
	TOTAL TIME	4.0 HR.



1-G SKYLAB CONFIGURATION POTENTIAL GSE REQUIREMENTS

- O BIOLOGICAL ISOLATION GARMET
- O CLEAN UP EQUIPMENT
 - o BRUSHES
 - o WIPES
 - o BIOCIDE/CLEANER
 - o TRASH BAGS
- FLUID CIRCULATION AND FLUSH SYSTEM (FOR FLUSHING OUT URINE SYSTEM)
- o STANDARD TOOLS
- o TRANSPORT CONTAINER



1-G SKYLAB CONFIGURATION POWER CONSUMPTION

Fan/Separator (Existing) 100W Air 200W Air/Liq

Processor Htr (if Req'd) 86W Peak 30W Avg.

Total Max

286W

44



1-G SKYLAB CONFIGURATION FILTER SIZING

Assumptions

- \bullet ΔP Same as Present Bag = 0.6 in H₂O at 30 CFM
- Laminar Flow Through Filter Material
- Test Results of Pall Filter Material $\Delta P = 4.9$ in H₂O, Q = 28 CFM, As 1/20 Ft² = .05 Ft²
- **■** Calculations:

 $\Delta P = K \ Q/A \ or \ K = \Delta PA/Q \ K = 4.9 \times .05/28 = .00875$ Bag Area A = .00875 Q × 144/ ΔP = .00875 × 30 × 144/.6 = 63 ln.²

Use Two 8 in. × 4 in. Filters



1-G SKYLAB CONFIGURATION

Expendables; 56 Man-Days + Contingency

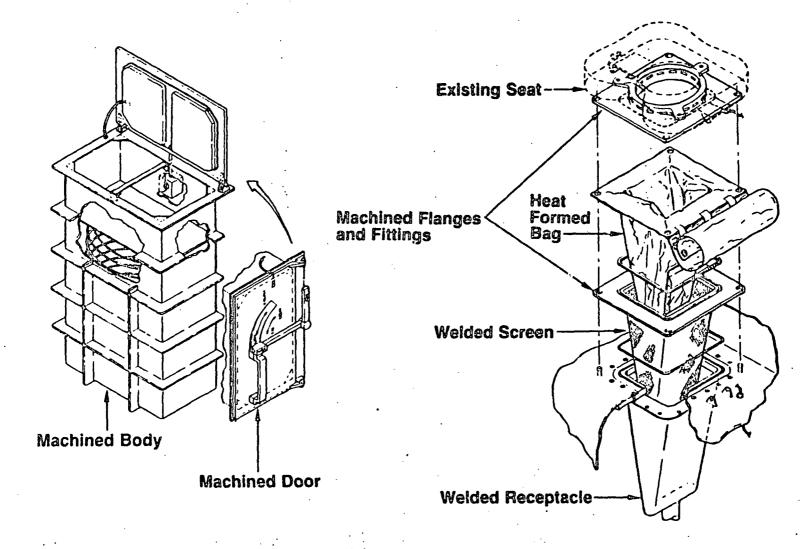
Total Bag Weight = Bag No. \times Weight/Bag = 75×2.2 lb = 17.0 lb

Overboard Air Loss = No. of Uses \times Air Loss Per Use Air Loss/Use = Processor Volume \times Air Density = 1.62 Ft³ \times .0752 lb/Ft³ = .122 lb

Total Air Loss Overboard (Max) = $75 \times .122$ lb = 9.14 lb



1-G SKYLAB CONFIGURATION HARDWARE FABRICATION FEASIBILITY



47



1-G SKYLAB CONFIGURATION BAG COST

Skylab Bag Cost = \$100/Bag in 1972

Add Inflation Factor of 2.90 From 1972 to 1985

Cost of 75 New Bags = \$100 × 2.90 × 75 = 21,750.00

Bag Cost Per Mission



1-G SKYLAB CONFIGURATION DEVELOPMENT ITEMS

- **B** Heat Sealing Device
- **B** Heat Sealable Material Compatibility/Outgassing
- **B** Adjustment of Airflow/△P of System
- **© Compaction Plate/Spring Constant**



1-G SKYLAB CONFIGURATION REQUIREMENTS REVIEW

GENERAL REQUIREMENTS

- O AIRFLOW SEPARATES WASTE FROM CREWMEMBER
- O WASTES STORES IN PROCESSOR UNDER VACUUM

SPECIFIC REQUIREMENTS

- O MALE/FEMALE FECES AND URINE COLLECTION INTERFACES SAME AS EXISTING SYSTEM
- O INDIVIDUAL URINE CAPS PROVIDED
- $^{\circ}$ O USE TIME EXCEEDS THAT OF EXISTING SYSTEM BY ONLY 1-1/2 MINUTES (APPROX.)
- O PAPER IS DEPOSITED INTO FECAL COLLECTOR DURING USE
- $^{f o}$ O CREW TRAINING SIMILAR TO CURRENT CONTINGENCY MODE OPERATIONS WITH SIMPLIFICATIONS
- O CREW HANDLES ONLY CLEAN OR SEALED BAGS
- O SEPARATION METHOD IDENTICAL TO EXISTING SYSTEM
- O BODY STABILIZATION SAME AS EXISTING SYSTEM
- **O CAPACITY FOR 56 BAGS (7 MAN X 8 DAY) PLUS 12% TO 34% (6 TO 19 BAGS) CONTINGENCY (ASSUMING BAGS ARE BETWEEN 0.40 AND 0.33 INCHES THICK)
 - O BACTERIA AND ODOR CONTROLLED BY VACUUM STORAGE AND ODOR FILTERS
 - O NOISE LEVEL EQUIVALENT TO EXISTING SYSTEM
 - O MAINTENANCE IS IN-VEHICLE
- O WEIGHT, POWER AND EXPENDABLES ARE LESS THAN OR EQUAL TO EXISTING SYSTEM
- O MECHANICAL AND ELECTRICAL SYSTEMS ARE SIMPLIFIED TO INCREASE RELIABILITY
- O SYSTEM IS RETROFITTABLE INTO ORBITER

^{*}DIFFERS FROM EXISTING SYSTEM

^{**}PER REDIRECTION OF D. GERMANY DURING MIDTERM REVIEW



1-G SKYLAB CONFIGURATION WEIGHT ESTIMATE SUMMARY

Component	Wt (lb)
Collector Receptacle	1.0
Mesh Screen Liner	0.4
1 Processor (Enlarged 50%)	27.0
1 Storage Compartment	6.0
Seat + Heat Sealer	5.0
Structural Supports	14.0
Switches, Cables, Elect. Conn.	3.0
Odor Bacteria Filter*	6.0
Restraint System*	7.0
2 Fan/Separators*	5.0
Hoses, Ducts*	5.0
Hardware Total	79.4
75 Bags**	17.0
Air** (75 Uses)	<u> </u>
Total System Wt	105.5 lb

^{*}Existing System Hardware **Expendables



WCS WEIGHT ESTIMATE SUMMARY (POUNDS)

System	Man- Days	Hdwe	Bags	Air	Liquid	Total
1-G Skylab	56	79.4	17.0	9.1	0	105.5
Centrifugal Comp	56	112.0	1.5	14.1	0	127.6
Centrifugal Comp	210	112.0	1.5	52.9	0	166.4
Skylab Repackaged	210	110.4	52.3	24.6	0	187.3
Modified Skylab	210	85.3	4.0	7.0	0	96.3
Closed Loop Macerator	210	88.5	0	0	93.6	182.1
Existing System	56	109.0	1.5	10.1	0	120.6
Existing System	210	109.0	1.5	37.9	0	148.4



1-G SKYLAB CONFIGURATION SUMMARY

ADVANTAGES

- 1. Skylab Collection Method Is Proven
- 2. Hardware Is Practical and Proven
- 3. Valves and Airflow System are Simple and Straightforward
- 4. Unit is Immediately Retrofittable Into Orbiter Structure and Interfaces
- 5. Air Loss Is Low Due to Smaller Processor Volume
- 6. Compaction and Heat Application are a Feature of Processor
- 7. Advanced Bag Sealing Concept Assures That Handling Is Limited to Clean or Sealed Bags
- 8. Existing Fan/Separators are Used
- 9. Direct Valve Linkages are Mechanically Simple
- 10. Unit Is Serviceable on Orbit
- 11. Odor Is Contained by Airflow During Bag Sealing
- 12. Used Bag Processing and Storage Occur in Same Chamber
- 13. Odor From Used Bags in Processors Is Contained by Airflow During Bag Insertion
- 14. Orderly Used Bag Storage in Processors Is More Volume Efficient and Simplifies Ground Changeout
- 15. Fresh Bag Stowage Area Is Provided
- 16. Sized to Accomodate Orbiter Mission and Crew Requirements

DISADVANTAGES

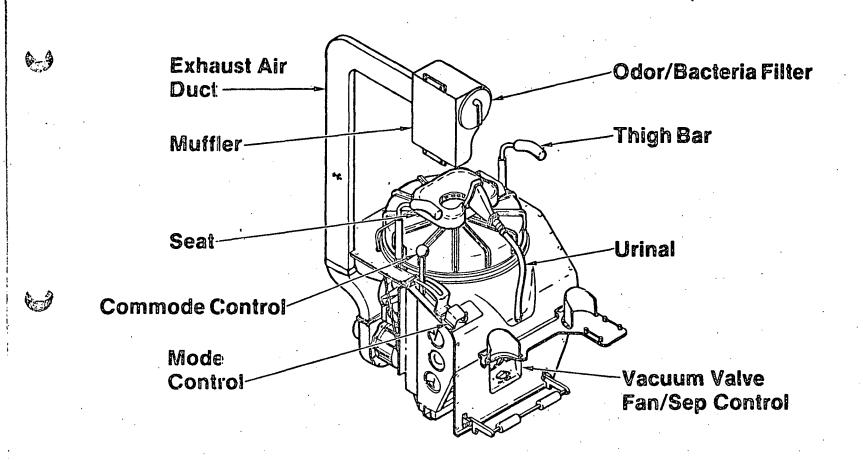
1. Fecal Bag Handling and Sealing are Present



CENTRIFUGAL COMPACTION CONCEPT

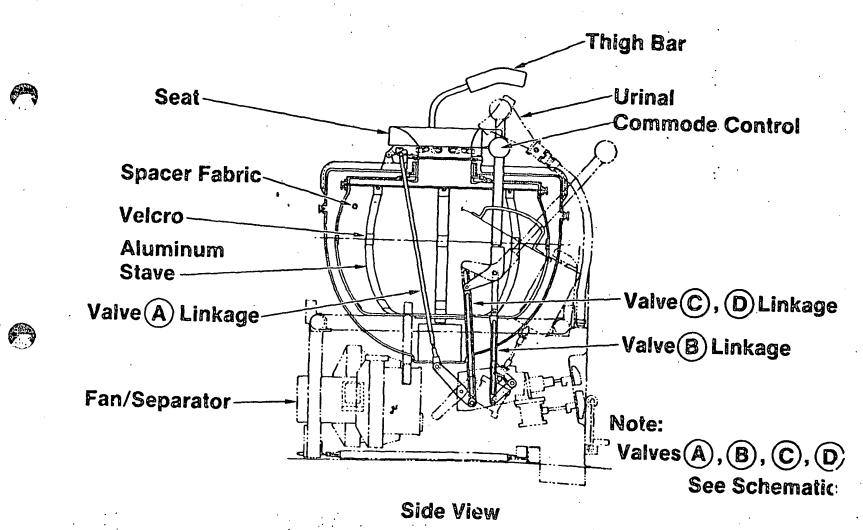


CENTRIFUGAL COMPACTION CONCEPT



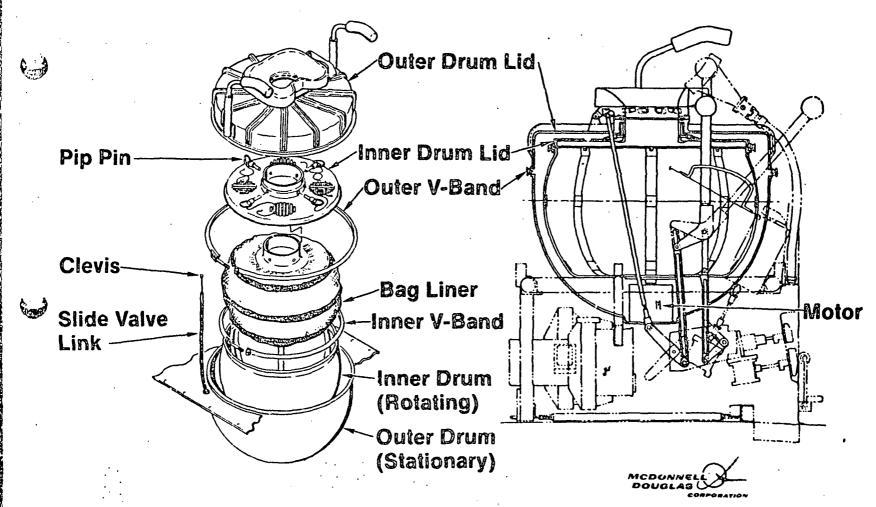


CENTRIFUGAL COMPACTION CONCEPT



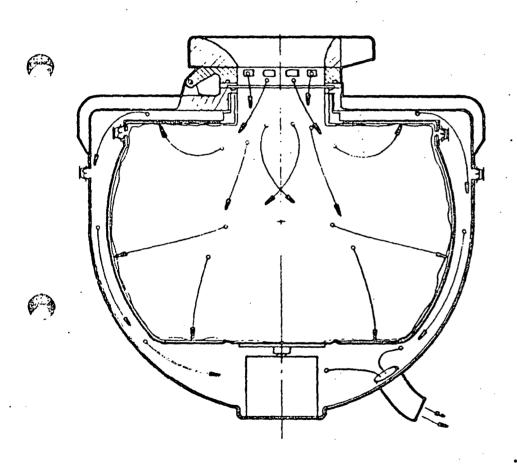
CENTRIFUGAL COMPACTION CONCEPT COLLECTION AND PROCESSING CHAMBER

VEC941





CENTRIFUGAL COMPACTION CONCEPT COLLECTION

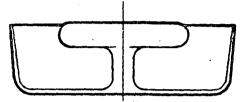


- Bolus Entrained by Airflow From Holes Around Base of Seat
- Inner Drum Rotates —
 Airflow and Centrifugal
 Force Move Bolus Toward
 Bag Liner
- Waste Is Compacted Against Inner Drum Wall — Center Collection Area Is Open
- Air Flows Out Through Bag,
 Spacer Fabric, Vents, and
 Outlet at Bottom

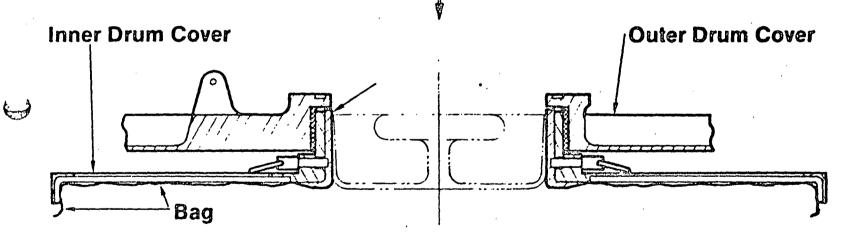
Rotation Speed	Compaction Force
1 RPS	1 G Approx
2 RPS	4 G Approx
3 RPS	12 G Approx



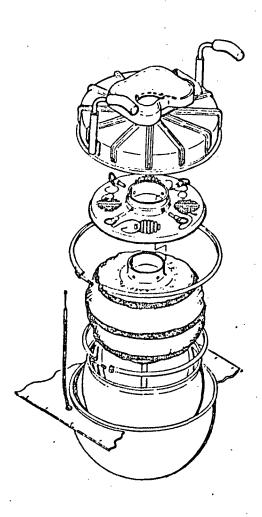
CENTRIFUGAL COMPACTION CONCEPT BAG PLUGGING



Stopper/Sealing Plug
Used Prior to
Bag Replacement



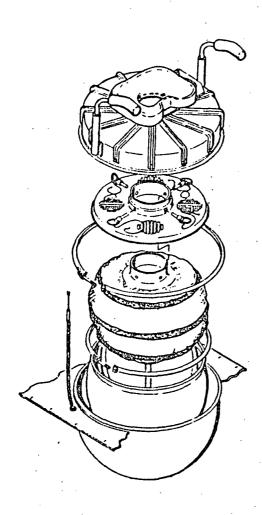
CENTRIFUGAL COMPACTION CONCEPT BAG REMOVAL



- **a** Raise Seat
- Unfasten Slide Valve Clevis
 From Slide Valve and Swing
 Slide Valve Link Out of the Way
- **a Lower Seat**
- Remove Outer V-Band Clamp
- Remove Outer Drum Lid
- Remove Inner V-Band Clamp
- Remove Inner Drum Lid and Bag Liner From Inner Drum
- Remove Pip Pins From Neck of Inner Drum Lid
- Detach Bag Liner From Underside of Inner Drum Lid



CENTRIFUGAL COMPACTION CONCEPT BAG INSTALLATION

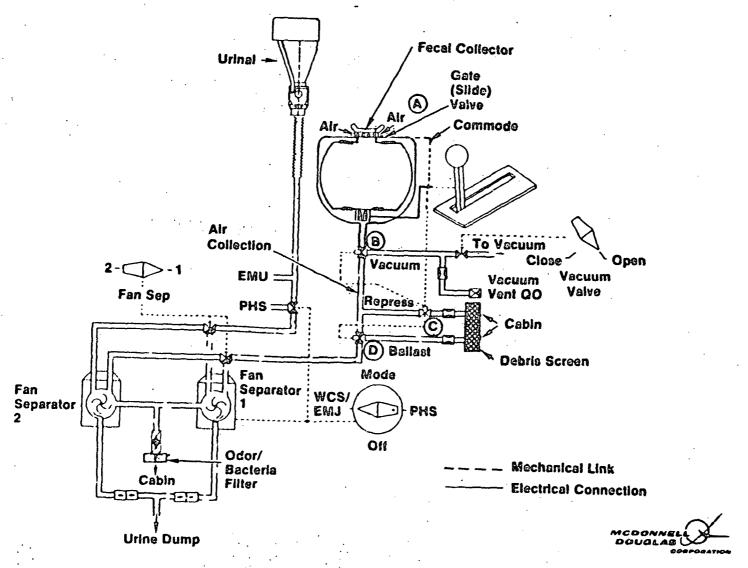


- Insert Neck of Fresh Bag Into Underside of Inner Drum Lid
- Replace Pip Pins
- Insert Bag Into Inner Drum,
 Secure Velcro Attachment
 Points
- Align Inner Drum Lid and Replace Inner V-Band Clamp
- Align Outer Drum Lid and Replace Outer V-Band Clamp
- Raise Seat
- Re-Attach Slide Valve Clevis and Linkage to Slide Valve
- **a** Lower Seat

MCDONNELL DOUGLAG

CENTRIFUGAL COMPACTION CONCEPT SYSTEM SCHEMATIC

VEC856





CENTRIFUGAL COMPACTION CONCEPT VALVE POSITIONS (SEE SCHEMATIC)

6.3

Mode-Off

- (A) Closed
- (B) Open to Vacuum
- © Open
- (D) Open to Ballast Line

Urine Collection: Model-WCS/EMU

- (A) Closed
- (B) Open to Vacuum
- © Open
- (D) Open to Ballast Line

Urine/Feces Collection: Mode-WCS/EMU

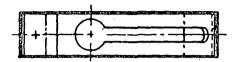
- Handle Up
 - (A) Closed
 - **B**Open to Air Collection Line
 - **©**Open
 - (D)Open to Ballast Line

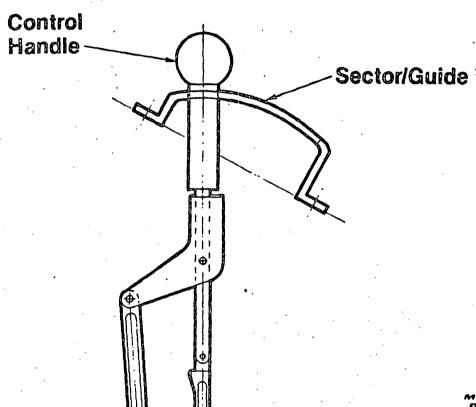
B Handle Forward

- (A) Open
- **(B)** Open to Air Collection Line
- (C) Closed
- (D) Open to Commode

CENTRIFUGAL COMPACTION CONCEPT VALVE LINKAGE IMPROVEMENT

VEC921



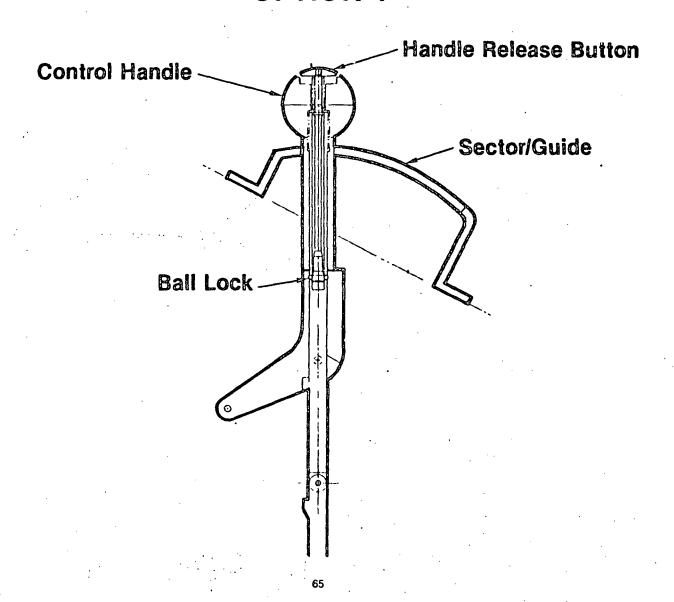


MCDONNELL



VALVE LINKAGE IMPROVEMENT OPTION 1

VEC922





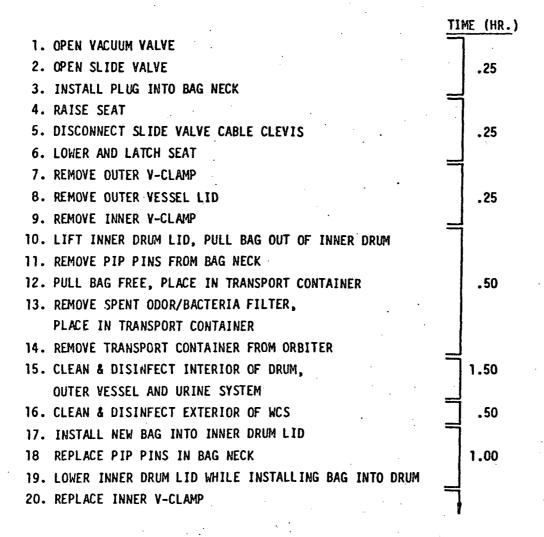
CENTRIFUGAL COMPACTION CONCEPT CREW PROCEDURES

TYPICAL USE CYCLE		CREW TIME		
		MIN. SEC.		
1.	TURN MODE SWITCH TO WCS/EMU*	2		
2.	PULL UP ON COMMODE CONTROL	. 3		
3.	POSITION BODY AND RESTRAINT SYSTEM	. •		
	WHILE WAITING (20 SECONDS MIN.)	30		
4.	PUSH COMMODE CONTROL FORWARD	3		
5.	PERFORM DEFECATION AND CLEANUP	12 0		
6.	REMOVE RESTRAINT SYSTEM	15		
7.	PUSH COMMODE CONTROL TO REAR AND DOWN (OFF)	5		
8.	TURN MODE SWITCH TO OFF	2		
9.	DISINFECT SEAT (STOW PAPER IN WET TRASH)	30		
	TOTAL TIME .	13 MIN. 30 SEC.		

*FOR URINATION ONLY (AFTER STEP 1), PROCEED TO PERFORM URINATION AND CLEANUP AND GO TO STEP 8.

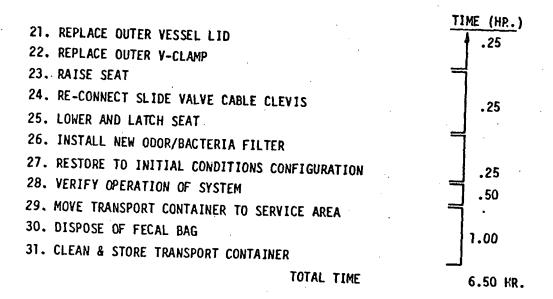


CENTRIFUGAL COMPACTION CONCEPT GROUND TURNAROUND





CENTRIFUGAL COMPACTION CONCEPT GROUND TURNAROUND (CONTINUED)





6

CENTRIFUGAL COMPACTION CONCEPT POTENTIAL GSE REQUIREMENTS

- O BIOLOGICAL ISOLATION GARMET
- O CLEAN UP EQUIPMENT
 - o BRUSHES
 - o WIPES
 - o BIOCIDE/CLEANER
 - o TRASH BAG
- o FLUID CIRCULATION AND FLUSH SYSTEM (FOR FLUSHING OUT URINE SYSTEM)
- o STANDARD TOOLS
- o TRANSPORT CONTAINER



CENTRIFUGAL COMPACTION CONCEPT POWER CONSUMPTION

- Fan/Separators (Existing) 100W Air 200W Air/Liq.
- Drum Motor 40W Max
 - Modify Existing Flight Qualified Slinger Motor
 - Add a 39:1 Reduction Gear Box



0.5

CENTRIFUGAL COMPACTION CONCEPT

Bag Pressure Drop:

• Bzg Approximately Same Area as Existing Bag Δ Pmax = 6 in. H₂O at 30 CFM

Overboard Air Loss:

- Air Loss Per Usage = Volume × Air Density = 3.35 ft³ × 0.0752 lb/ft³ = 0.252 lb
- Total Air Loss for 210 Man Day Uses
 = Man Days × Air Loss/Usage = 210 × 0.252 lb = 52.9 lb
- Total Air Loss for 56 Man Day Uses
 = Man Days × Air Loss/Usage = 56 × 0.252 lb = 14.1 lb



6

CENTRIFUGAL COMPACTION CONCEPT

- Sizing of Rectangular Exhaust Air Duct Extension To Have Same ΔP as Present 1.5 in OD Duct
 - Let Outside Width (W) = 1 in. for Personal Hygiene Tray Clearance. Wall Thickness = 0.030 in.
 - Let Hydraulic Dia.,(DH) = 4 × Area (A)/Perimeter (S), Equal Diameter of Round Duct
 - ID of Round Duct \times 1.5 0.060 = 1.44 in. Inside Width (WINS) of Rect. Duct = 1 0.060 = 0.94 in.

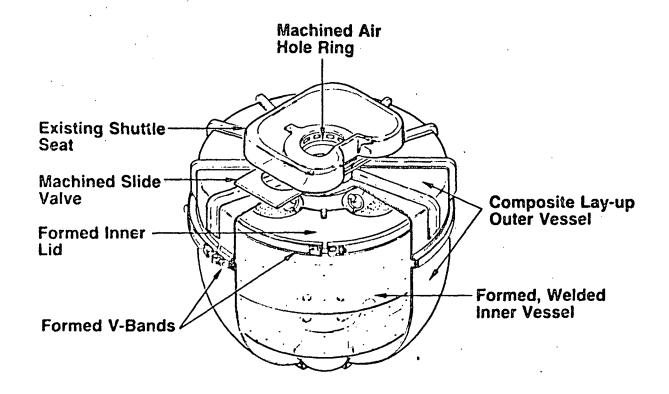
LINS =
$$\frac{DH \text{ WINS}}{(2 \text{ WINS} - DH)} = \frac{1.44 \times 0.94}{2 \times 0.94 - 1.44} = 3.08 \text{ in.}$$

Outside Dimensions = 1 in \times (3.08 + 0.060) = 1 in. \times 3.14 in.

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CENTRIFUGAL COMPACTION CONCEPT HARDWARE FABRICATION FEASIBILITY



Bag: Porous Filter Medium Bonded at Joints

VEC861

CENTRIFUGAL COMPACTION CONCEPT DEVELOPMENT ITEMS

■ Motor Drive/Gearbox

B Rotating Bearing

■ Drum Spin Speed



CENTRIFIGUAL COMPACTION CONCEPT REQUIREMENTS REVIEW

GENERAL REQUIREMENTS

- O AIRFLOW SEPARATES WASTE FROM CREWMEMBER
- O WASTES STORED EN MASSE IN VACUUM CONTAINER

SPECIFIC REQUIREMENTS

- O MALE/FEMALE FECES AND URINE COLLECTION INTERFACES SAME AS EXISTING SYSTEM
- O INDIVIDUAL URINE CAPS PROVIDED
- O CREW PROCEDURES IDENTICAL TO EXISTING SYSTEM
- O PAPER IS DESPOSITED INTO FECAL COLLECTOR DURING USE
- O CREW TRAINING IDENTICAL TO EXISTING SYSTEM
- O NO HANDLING OF WASTE
- O SEPARATION METHOD IDENTICAL TO EXISTING SYSTEM
- O BODY STABILIZATION SAME AS EXISTING SYSTEM
- O CAPACITY EQUAL TO EXISTING SYSTEM WITH COMPACTION CAPABILITY ADDED
- O BACTERIA AND ODOR CONTROLLED BY VACUUM STORAGE AND FILTERS
- O NOISE LEVEL EQUIVALENT TO EXISTING SYSTEM
- O MAINTENANCE IN VEHICLE
- O WEIGHT, POWER, AND EXPENDABLES ARE EQUIVALENT TO EXISTING SYSTEM
- O VALVE MECHANISM RELIABILITY IS INCREASED; ROTATING CHAMBER IS DESIGNED WITH FAIL-OPERATIONAL CHARACTERISTICS
- O SYSTEM IS RETROFITTABLE INTO ORBITER

^{*}DIFFERS FROM EXISTING SYSTEM



CENTRIFUGAL COMPACTION CONCEPT WEIGHT ESTIMATE SUMMARY

Component	Wt (lb)	
Inner Drum	11.0	
Outer Drum (Composite)	41.0	
Slide Valve	3.0	
Seat	3.0	
Motor	3.0	
Structural Supports	14.0	
Switches, Cables, Elect. Conn.	7.0	
Odor Bacteria Filtcr*	6.0	
Restraint System*	7.0	
Fiberglass Shroud	7.0	
2 Fan/Separators*	5.0	
Hoses, Ducts*	5.0	
Hardware Total	112.0	
Bags**	1.5	
Air**	_52.9	14.1
Total System Wt	166.4	127.6
*Existing System Hardware **Expendables	210 Uses	56 Uses



WCS WEIGHT ESTIMATE SUMMARY (POUNDS)

System	Man- Days	Hdwe	Bags	Air	Liquid	Total
1-G Skylab	56	79.4	17.0	9.1	0	105.5
Centrifugal Comp	56	112.0	¹ 1.5	14.1	0	127.6
Centrifugal Comp	210	112.0	1.5	52.9	0	166.4
Skylab Repackaged	210	110.4	52.3	24.6	0	187.3
Modified Skylab	210	85.3	4.0	7.0	0	96.3
Closed Loop Macerator	210	88.5	0	0	93.6	182.1
Existing System	56	109.0	1.5	10.1	0	120.6
Existing System	210	109.0	1.5	37.9	0	148.4



CENTRIFUGAL COMPACTION CONCEPT SUMMARY

ADVANTAGES

- 1. Collector Mounts Directly Onto Existing Commode Structure Which Is Immediately Retrofittable Into Orbiter Compartment
- 2. Existing Fan/Separators, Valves, Hardware and Interfaces are Used
- 3. Commode Control and Valve Linkage is improved
- 4. Compaction of Tissues and Fecal Material Is Provided By Centrifugal Force
- 5. Rotation Moves Fecal Material Out of View of Crew
- 6. Large Bag Collection Method Is Simple and Proven
- 7. Low Rotation Speed Enhances Mechanical and Functional Reliability.
- 8. Motor and Rotating Drum Revert to Simple Bag Operation in Event of Failure
- 9. Motor and Shaft Located Within Pressure Vessel Eliminates Need for a Rotating Seal Around Shaft
- 10. Crew Handles No Waste
- 11. Waste Material Is Deactivated by Vacuum Drying and/or Freezing
- 12. Air Loss Similar to Current System
- 13. Complete Enclosure of Bag Minimizes Stress on Bag Material
- 14. Plug Provides for Simple, Positive, and Hygienic Closure of Bag for Convenient and Sanitary Ground Handling
- 15. Big Bag Concept Eliminates Bag Handling for Shuttle Application
- 16. Bag May be Easily Changed on Orbit for a Longer Duration Space Station Mission

DISADVANTAGES

- 1. Rotating Bearing at Bag Opening Is Required
- 2. An Out of Balance Condition Due to Non-Uniform Buildup of Fecal Material May Lead to Bearing Wear or the Need for a Balancing Device



TASK 5 PROGRAM REVIEW REQUIREMENTS

VEC912

- m Initial Subsystem Review at JSC
- Mid-Term Status Review at MDAC-HB
- a Formal Presentation at JSC



TASK 6 PROGRAM DOCUMENT REQUIREMENTS

VEC913

5 Final Report



APPENDIX A SPACE STATION WCS CONCEPT

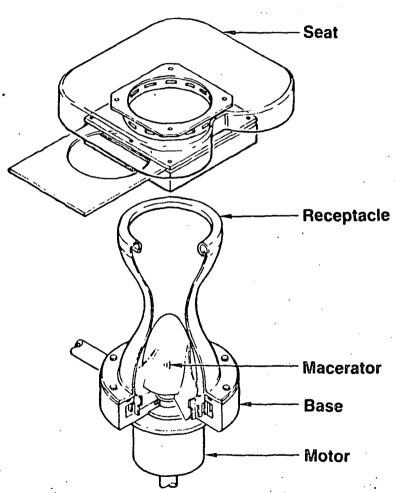


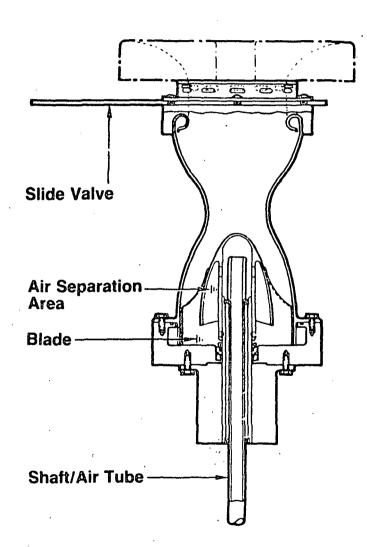
CLOSED LOOP MACERATOR SYSTEM CONCEPT

VEC865

CLOSED LOOP MACERATOR CONCEPT



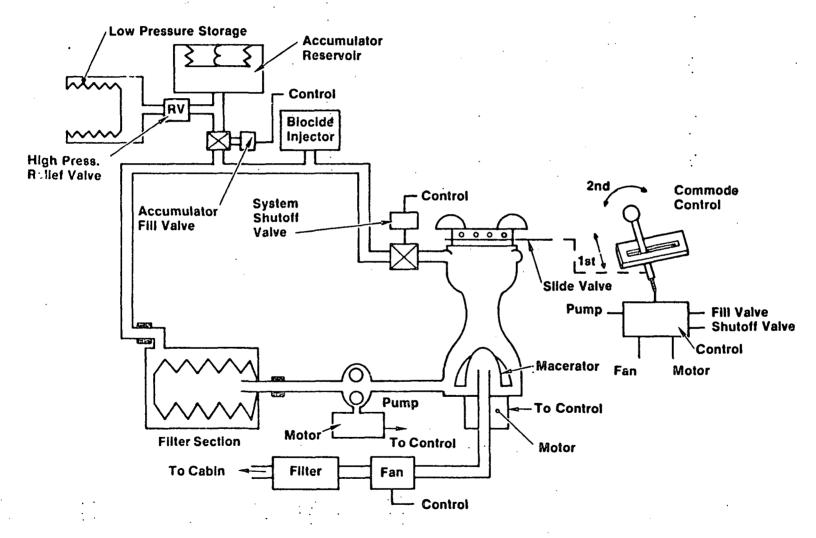




VEC866



CLOSED LOOP MACERATOR SYSTEM CONCEPT SYSTEM SCHEMATIC



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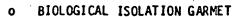


CLOSED LOOP MACERATOR SYSTEM CONCEPT GROUND OPERATIONS

- 1. Close filter isolation valves
- 2. Disconnect bellows/filter unit
- 3. Place bellows/filter unit in transport container
- 4. Remove transport container from orbiter
- 5. Connect fluid flush/recharge system to line shutoff valve connectors
- 6. Open line shutoff valves and flush out system to disinfect
- 7. Cycle volume control reservoir, biocide injector, and slurry pump while flushing
- 8. Stop flushing momentarily, open slide valve
- 9. Inspect slide valve, clean if necessary, close
- 10 Continue flushing to clear system of slide valve debris
- 11. When fluid is clear, fill volume control reservoir
- 12 Stop flushing, close filter isolation valve
- 13. Disconnect fluid flush system
- 14. Install new fluid charged bellows/filter unit
- 15. Open filter isolation valves
- 16. Recharge biocide injector
- 17. Install new odor/bacteria filter
- 18. Verify system back to initial conditions
- 19. Service bellows/filter unit as necessary



CLOSED LOOP MACERATOR SYSTEM CONCEPT POTENTIAL GSE REQUIREMENTS



- ODOR/BACTERIA FILTER
- O RECHARGED BELLOWS/FILTER UNIT
- O CLEAN UP EQUIPMENT
 - a BRUSHES
 - o WIPES
 - o BIOCIDE/CLEANER
 - o TRASH BAGS
- o FLUID CIRCULATION AND FLUSH/RECHARGE SYSTEM
- o STANDARD TOOLS
- TRANSPORT CONTAINER
- O SERVICING EQUIPMENT FOR BELLOHS/FILTER UNIT



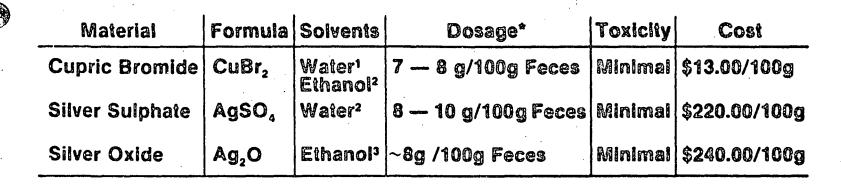
CLOSED LOOP MACERATOR SYSTEM EXPENDABLES SUMMARY

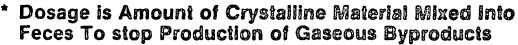
No Expendables

- Air Used Only for Collection and Entrainment Recirculated Back to Cabin Through Odor/Bacteria Filter
- Liquid Used Only to Circulate Fecal Material and Carry
 Biocide for Deactivation Recirculated Through System and Filter

CLOSED LOOP MACERATOR SYSTEM Biocide Data

VEC881





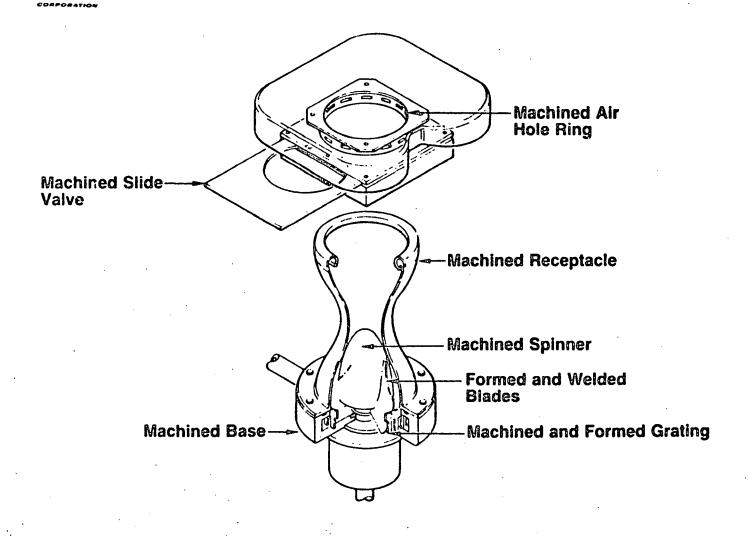
1 Very Soluble

2 Moderately Soluble

3 Low Solubility

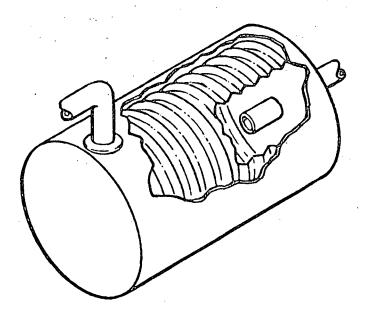
MCDONNELL DOUGLAS

CLOSED LOOP MACERATOR CONCEPT HARDWARE FABRICATION FEASIBILTY



CLOSED LOOP MACERATOR CONCEPT HARDWARE FABRICATION FEASIBILITY (CONT'D)

TBD



Filter Section

MCDONNELL DOUGLAS



CLOSED LOOP MACERATOR CONCEPT DEVELOPMENT ITEMS

- Macerator/Separator
- **E** Collection Bowl
- **B** Filter Section
- Macerator Motor and Seals
- **Slurry Pump**
- **B Volume Control Reservoir**
- **B** Sensors
- Biocide Quantity and Type
- Adjustment of Flow/△P Characteristics of System



CLOSED LOOP MACERATOR SYSTEM WEIGHT ESTIMATE SUMMARY

Component	Wt (lb)
Collector Vessel	3.1
Seat Adapter	0.5
Bottom Plate	0.5
Macerator Blades	0.3
Spinner	2.3
Seat	3.0
Slide Valve	3.0
Motor	3.0
Slurry Pump	4.0
Filter Section	31.2
Accumulator, Injector, Valving	10.0
Piping	10.0
Structural Supports	14.3
Switches, Cables, Elect. Conn.	<u>2.6</u>
Hardware Total	88.5
Fluid	93.6
Total System Wt	182.1



WCS WEIGHT ESTIMATE SUMMARY (POUNDS)

System	Man- Days	Hdwe	Bags	Air	Liquid	Total
1-G Skylab	56	79.4	17.0	9.1	0	105.5
Centrifugal Comp	56	112.0	1.5	14.1	0	127.6
Centrifugal Comp	210	112.0	1.5	52.9	0	166.4
Skylab Repackaged	210	110.4	52.3	24.6	0	187.3
Modified Skylab	210	85.3	4.0	7.0	0	96.3
Closed Loop Macerator	210	88.5	0	0	93.6	182.1
Existing System	56	109.0	1.5	10.1	0	120.6
Existing System	210	109.0	1.5	37.9	0	148.4



CLOSED LOOP MACERATOR SYSTEM

ADVANTAGES

- 1. Configuration is Applicable to Space Station
- 2. Air and Water Entrainment is More Effective Than Air Alone
- 3. Crew Use Time is Minimal-Similar to Conventional Toilet
- 4. Crew Training Time is Minimal
- 5. Waste is Flushed Completely Out of Sight
- 6. Water Continually Cleans Collection Surface During Use
- 7. Unit is Psychologically Very Acceptable
- 8. Biocide is Thoroughly Mixed With Feces to Provide Deactivation
- 9. No Air Loss Closed System
- 10. Entire System Operates in a Cabin Pressure Environment
 11. Compaction and Containment Capability are Provided by a Macerator and Filter
- 12. Filter Section is Self Contained and Can be Hygienically Changed Out on Orbit or Ground
- 13. With Removal of Filter Only, Entire Unit Can be Flushed Out on Ground
- 14. Use of Slide Valve Permits More Flexibility in Choice of Biocide Scent is **Isolated From Cabin Environment**

DISADVANTAGES

- 1. A Biocide Which is Effective Yet Non-Toxic to Crew Must be Found
- 2. Macerator/Air Separator Requires Development
- 3. Filtration Section Requires Development
- 4. Development Cost May be High
- 5. System is Somewhat Complex Due to Mechanical, Electrical, and Sensing Devices

MCDONNELL DOUGLAS CORPORATION

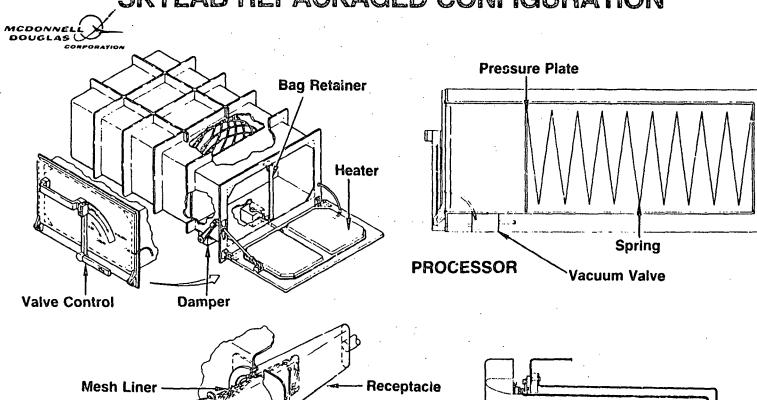
APPENDIX B

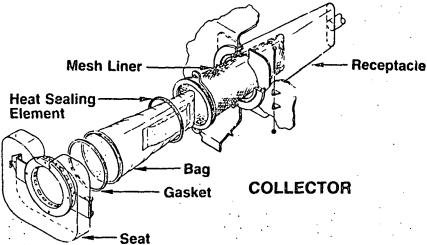
Other Semi-Final Concepts

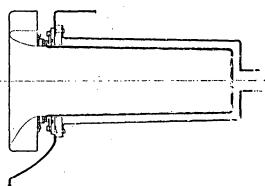


SKYLAB REPACKAGED CONFIGURATION

SKYLAB REPACKAGED CONFIGURATION

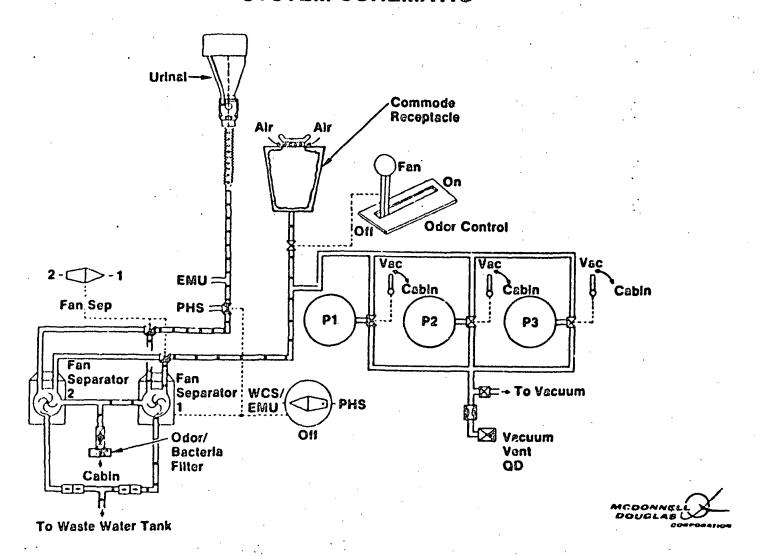






SKYLAB REPACKAGED CONFIGURATION SYSTEM SCHEMATIC

VEC886





SKYLAB REPACKAGED CONFIGURATION

	CREW PROCEDURES	CREW	TIME
		Min.	Sec.
1.	Turn on air collection system	,	2
2.	Position body and restraint system		30
3.	Perform defecation and cleanup	12	0
4.	Remove restraint system		15
5.	Unlatch and lift seat		10
6.	Seal bag		15
7.	Verify or close processor vacuum valve,		
	wait for repressurization	,	5
8.	Open processor door		5 .
9.	Remove bag from collector		5
10.	Place bag into processor		15
11.	Close processor door		5
12.	Open processor vacuum valve	•	3
13.	Disinfect seat		30
14.	Open clean bag dispenser		5
15.	Install clean bag		15
16.	Close clean bag dispenser		5
17.	Lower seat & latch		10
18.	Turn off air collection system		2
	Total time	14 Min	. 57 Sec.



SKYLAB REPACKAGED CONFIGURATION GROUND OPERATIONS

- Attach filter (GSE*) to vacuum line(s)
- 2. Start cabin ventilation fan
- Open vacuum line(s) to atmosphere
- 4. Open processor door(s)
- 5. Remove bags, place into air-tight transport container
- 6. Remove spent odor/bacteria filter
- 7 Place filter in transport container
- 8. Remove transport container from orbiter
- 9. Clean & disinfect interior of collector, processors and vacuum system
- 10. Clean & disinfect exterior of WCS
- 11. Install fresh bag
- 12. Install fresh odor/bacteria filter
- 13. Return system to initial condition configuration
- 14. Remove filter (GSE) from vacuum line(s)
- 15. Move transport container to service area
- 16. Remove waste from transport container
- 17. Clean & store transport container

^{*}Ground Support Equipment



SKYLAB REPACKAGED CONFIGURATION POTENTIAL GSE REQUIREMENTS

- O BIOLOGICAL ISOLATION GARMET
- O ODOR/BACTERIA FILTER
- O CLEAN UP EQUIPMENT
 - o BRUSHES
 - o WIPES
 - o BIOCIDE/CLEANER
 - o TRASH BAGS
- FLUID CIRCULATION AND FLUSH SYSTEM (FOR FLUSHING OUT VACUUM LINES AND AIR FLOW SYSTEM)
- o STANDARD TOOLS
- O TRANSPORT CONTAINER

SKYLAB REPACKAGED CONFIGURATION

· AIR LOSS = USES X PROCESSOR VOL X AIR DENSITY (STD WAD)

= 210 USES
$$\times \frac{1.55 \text{ ft}^3}{\text{USE}} \times \frac{0.752 \text{ LB}}{\text{ft}^3} = 24.6 \text{ LB}$$

· BAG WEIGHT = NO. OF BAGS X WT PER BAG X CONTINGENCY FACTOR



VEC876

SKYLAB REPACKAGED CONFIGURATION HARDWARE FABRICATION FEASIBILITY

MCDONNELL DOUGLAS CORPORATION

COLLECTOR (EXISTING)

Welded Screen

Welded Receptacle

Heat Formed Bag

Machined Flanges

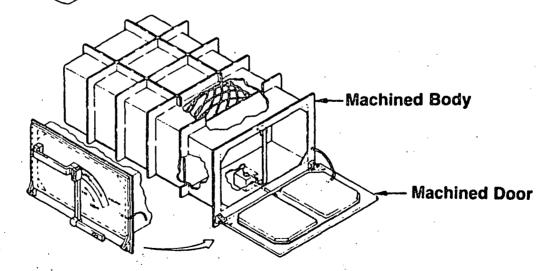
and Fittings

Machined Ring With-Air Holes

Seat

Existing Shuttle-

PROCESSOR (RE-CONFIGURED)





SKYLAB REPACKAGED

ANALYSES TO BE COMPLETED BY END OF DESIGN PHASE

O AIRFLOW :

AP OF BAG FILTER MATERIAL

INTERACTION OF SYSTEM COMPONENTS -CORRECT FLOWS, ETC

O EXPENDABLES :

AIR LOSS (COMPLETED)
BAGS - VOLUME, WEIGHT (COMPLETED)

O CREW TIME :

CREW TIME LINES (COMPLETED)

O THERMAL :

HEAT TRANSFER OF BAG MATERIAL

MULTIPLE BAG EFFECTS ON DEACTIVATION

O STRUCTURAL: MOUNTING OF SYSTEM COMPONENTS ON ORBITER PRIMARY STRUCTURE

STRUCTURAL INTEGRITY OF COLLECTOR AND PROCESSORS

SYSTEM WEIGHT ESTIMATE (COMPLETED)

O MASS BALANCE: EFFECTS OF SYSTEM ON VEHICLE ORBITAL AND FLIGHT DYNAMICS

o POWER :

POWER CONSUMPTION OF FAN/SEPARATOR

POWER CONSUMPTION OF HEATER ELEMENT



SKYLAB REPACKAGED CONFIGURATION WEIGHT ESTIMATE SUMMARY

,	COMPONENT	WT (LB)
	COLLECTOR RECEPTACLE	1.0
	MESH SCREEN LINER	0.4
	4 PROCESSORS	47.0
	3 STORAGE COMPARTMENTS	19.0
	SEAT	3.0
	STRUCTURAL SUPPORTS	14.0
	SWITCHES, CABLES, ELECT. CONN.	3.0
	ODOR/BACTERIA FILTER *	6.0
	RESTRAINT SYSTEM *	7.0
	2 FAN-SEPARATORS*	5.0
	HOSES, DUCTS *	5.0
	HARDWARE TOTAL	110.4 52.3
	BAGS** AIR **	24.6
	TOTAL SYSTEM WT	187.3 LB

VEC875



ADVANTAGES

- 1. Storage Is Orderly Easier Ground Changeout
- 2. Processing and Storage Occur in Same Container
- 3. Skylab Collection Method Is Proven
- 4. Efficient Use of Shuttle Envelope
- 5. Low Air Loss Due to Smaller Volume of Processor
- 6. Compaction and Heat Application are a Feature of Processor
- 7. Crew Handles Only Clean or Sealed Bags With Advanced Bag Sealing Concept
- 8. Utilizes Existing Fan/Separator System
- 9. Mechanically Simple
- 10. Serviceable on Orbit
- 11. Airflow Is Used to Contain Odor During Bag Sealing
- 12. Airflow Is Used to Contain Odor From Processors During Bag Insertion
- 13. Stowage Area for Fresh Bags Is Provided

DISADVANTAGES

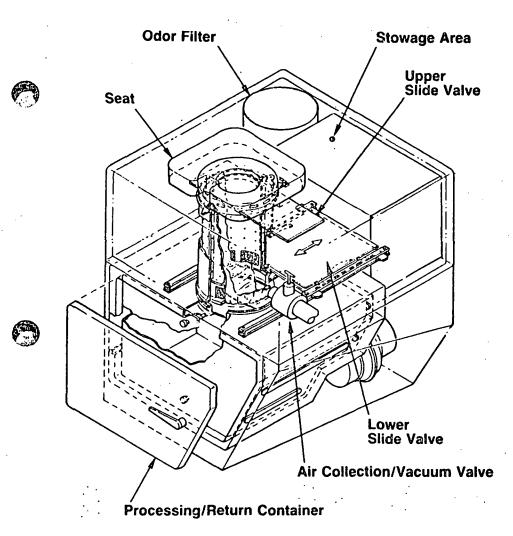
- 1. Fecal Bag and Associated Handling, Sealing, and Outgassing are Present
- 2. Required Bag Stowage Space Is Large but Adequate
- 3. Door to Personal Hygiene Compartment May Need to be Removed and a More Compact Restraining Device Installed
- 4. Use of Wall Towel Restraints and Personal Hygiene Stowage Compartment May be Lost on Orbiter
- 5. Space Station Applicability Is Low
- 6. Old Fecal Bags May Have to be Touched While Inserting Newly Used Bags Into Processor
- 7. Crew Acceptance May be Low

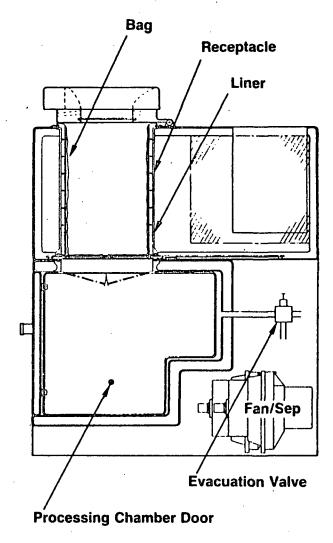


MODIFIED SKYLAB CONCEPT



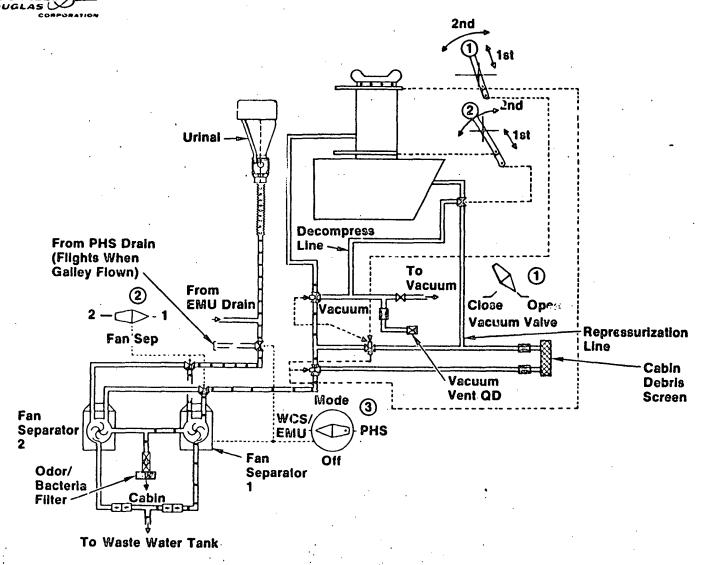
MODIFIED SKYLAB CONCEPT





MODIFIED SKYLAB CONCEPT SYSTEM SCHEMATIC

VEC888





MODIFIED SKYLAB CONCEPT CREW PROCEDURES

	·	CREW TIME
		Min. Sec.
1.	Verify or close vacuum valve 1,	· ·
	wait for repressurization	15
2.	Open slide valve l	5
3.	Turn on air collection system	2
4.	Position body and restraint system	30
5.	Perform defecation and clean up	12 0
6.	Remove restraints	. 15
7.	Close slide valve 1	5
8.	Turn off air collection system	. 2
9.	Open vacuum valve l	· 3
10.	Disinfect seat	30
	Total Time	13 Min. 47 Sec.



MODIFIED SKYLAB CONCEPT CREW PROCEDURES (CONTINUED)

	CREW TIME
BAG DISPOSAL	Min. Sec.
1. Close vacuum valve 1	15
2. Close vacuum valve 2	20
3. Turn on air collection system	2
4. Open slide valve l	5
5. Unlatch and lift seat	. 15
6. Seal bag	15
7. Obtain push through tool	10
8. Use push through tool to compact/deflate bag	20
9. Open slide valve 2	5
10. Push bag into return container	·
using push through tool	15
11. Close slide valve 2	5
12. Turn off air collection system	2
13. Install new bag in receptacle	15
14. Lower seat and latch	15
15. Close slide valve 1	5
16. Open vacuum valve 1	5
17. Cpen vacuum valve 2	5
Total Time	2 Min. 54 Scc.



MODIFIED SKYLAB CONCEPT* GROUND OPERATIONS

- 1. Attach filter (GSE**) to vacuum line(s)
- 2. Vent vacuum line(s) to atmosphere
- 3. Open return container compartment door
- 4. Remove return container
- Install lid (GSE) on return container
- 6. Remove spent odor/bacteria filter
- 7. Briefly remove lid of return container
- 8. Place spent filter into return container
- 9. Re-cap return container
- 10. Remove return container from orbiter
- 11. Clean and disinfect interior of collector and return container compartment
- 12. Clean and disinfect exterior of WCS
- 13. Install a replacement return container
- 14. Install a new bag in receptacle
- 15. Install fresh odor/bacteria filter
- 16. Return system to initial conditions/configuration
- 17. Remove filter (GSE) from vacuum line(s)
- 18. Transport return container to service area
- 19. Remove waste from return container
- 20. Clean and store return container for future use

*Assumes no bag in collector area upon return to earth

** Ground Support Equipment



MODIFIED SKYLAB CONCEPT POTENTIAL GSE REQUIREMENTS

- o BIOLOGICAL ISOLATION GARMET
- o ODOR/BACTERIA FILTER
- O RETURN CONTAINER
- O CLEAN UP EQUIPMENT
 - o BRUSHES
 - o WIPES
 - o BIOCIDE/CLEANER
 - o TRASH BAG
- FLUID CIRCULATION AND FLUSH SYSTEM (FOR FLUSHING OUT VACUUM LINES AND AIR FLOW SYSTEM)
- o STANDARD TOOLS
- O VACUUM PUMP ASSEMBLY (FOR CONTINGENCY USE ONLY TO COMPLETE PROCESSING AND ALLOW EXAMINATION OF WCS EQUIPMENT WHILE WASTE IS STILL PRESENT)

MCDONNELL DOUGLAS CONFORMATION

MODIFIED SKYLAB CONCEPT

· AIR LOSS = LOSS DUE TO USE + LOSS DUE TO BAG CHANGE (STD COND)

= USES X VOL X AIR DENSITY + CHANGES X VOL X AIR DENSITY CHANGE

= 210 USES x . 34 FF 3 x . OTSZLB + 10 CHANGES X 2.19 FF 3 CHANGE X OTSZLB

= 5.4 LB + 1.6 LB = 7.0 LB

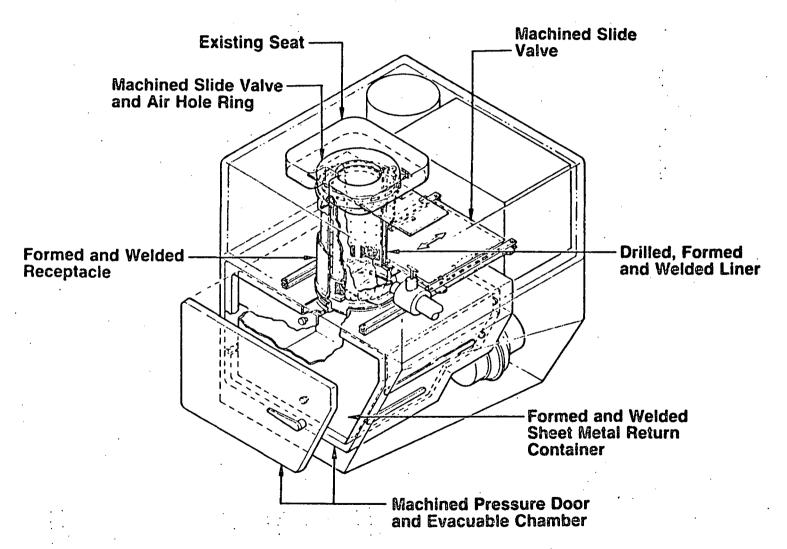
• BAG WEIGHT = WT PER BAG X NO OF BAGS X CONTINGENCY FACTOR

(ESTIMATE BAG WT = 162 9 PER BAG = .356 LB)

= .356 LB × 10 BAGS X 1.10 = 3.92 = 4.0 LB



MODIFIED SKYLAB CONCEPT HARDWARE FABRICATION FEASIBILITY



MODIFIED SKYLAB CONCEPT



ANALYSES TO BE COMPLETED BY END OF DESIGN PHASE

O AIRFLOW :

AP OF BAG FILTER MATERIAL

INTERACTION OF SYSTEM COMPONENTS -CORRECT FLOWS, ETC

O EXPENDABLES : AIR LOSS (COMPLETED)

BAGS - VOLUME, WEIGHT (COMPLETED)

O CREW TIME : CREW TIME LINES (COMPLETED)

O THERMAL : HEAT TRANSFER OF BAG MATERIAL AND RECEPTACLE /LINER

EFFECT OF MULTIPLE DEFECATIONS ON DEACTIVATION

O STRUCTURAL: MOUNTING OF SYSTEM COMPONENTS ON ORBITER PRIMARY STRUCTURE

STRUCTURAL INTEGRITY OF COLLECTOR AND EVACUABLE AREAS

SYSTEM WEIGHT ESTIMATE (COMPLETED)

O MASS BALANCE: EFFECTS OF SYSTEM ON VEHICLE ORBITAL AND FLIGHT DYNAMICS

O POWER : POWER CONSUMPTION OF FAN/SEPARATOR



MODIFIED SKYLAB CONCEPT Weight Estimate Summary

VEC889

Component	WT (Ib)
Collector Receptacle	2.3
Collector Liner	3.2
Upper Slide Valve	3.0
Lower [Double] Slide Valve	6.0
Seat	3.0
Return Container	6.1
Storage Chamber	26.2
Structural Supports	10.0
Switches, Cables, Elect. Conn.	2.5
Odor/Bacteria Filter*	6.0
Restraint System*	7.0
2 Fan/Separators*	5.0
Hoses, Ducts*	5.0
Hardware Total	85.3
Bags**	4.0
Air**	7.0
Total System Weight	96.3
* Existing System Hardware **Expendables	

VEC887



MODIFIED SKYLAB CONCEPT SUMMARY

Advantages

- 1. Periodic Bag Ejection Removes Waste From Cabin
- 2. Utilizes Existing Hardware Concepts
- 3. Low Air Loss During Evacuation of Collecting Chamber Between Defecations
- 4. Crew Operations Minimized by Extending Bag Use Period To Three Days
- 5. Fecal Material Deactivated by Vacuum and Heat Absorbtion Between Defecations
- 6. Serviceable On Orbit
- 7. Bag Push Through Done at Cabin Pressure Not a Remote Operation
- 8. Space Station Applicability
- 9. Moderate to Low Bag Consumption
- 10. Utilizes Existing Fan/Seperator System
- 11. Storage/Processing Area is Pressurized During Pass Through
- 12. Skylab Collection Method Is Proven
- 13. Airflow is Used to Contain Odor During Pass Through
- 14. Crew Handles Only Clean or Sealed Bags With Advanced Bag Sealing Concept

☑ Disadvantages

- 1. Fecal Material From Previous Defecations Will Be In View of Other Crew Members
- 2. Old Fecal Material in Bag May Obstruct Collection of New Waste
- 3. Fecal Bag and Associated Handling, Sealing, and Outgassing Are Present
- 4. Randomly Stored Bags Do Not Utilize Stowage Space Efficiently
- 5. Psychological Acceptance May Be Poor



APPENDIX C SKYLAB SYSTEM DATA



SKYLAB URINE/FECAL COLLECTOR Flow Schematic

Performance of Urine System Airflow Only — 1 CFM Δ P(A-C) = 1.9 In. H₂O Δ P(A-B) \approx 1 In. H₂O Urine Only — 45mL/SEC Δ P(A-B) \approx 1.8 In. H₂O No Flow — Max. Δ P(A-C) = 8 In. H₂O **B** Ürine Bag -Fecal Power Seat Switch /Fecal Bag Separator I Valve Odor Filter Valve Seat Drawer Fairchild Industries MDAC

Blower/Motor Assembly (1B83241)

Flow Rate (Nominal)

Fecal Urine

Differential Pressure at Flow Rate

Motor Input Voltage

Power

Steady Run Mode Starting Transient

Locked Rotor (Current limited)

Overload Protection (Circuit breaker)

Pressure Range

Nominal Operating Gas Inlet

Pressure

Temperature Range

Nominal Operating Operational Nonoperating (Storage)

Operational Life

Odor Removal Assembly (Charcoal bed)

Charcoal Weight

Flow Rate Across Bed

Differential Pressure at Flow Rate

Operating Pressure Range

Centrifugal Urine Separator Assembly (CUSA) (1887234)

Separator

Flow Rate Urine (Through inlet) Urine (Through outlet with

 $3 \pm 0.25 \text{ in. } H_2O \Delta P)$ Gas (Cabin air @ 5 psia)

Pressure Range Operating

Proof

Burst

10.4 cfm⁽⁴⁾, 8.7 to 9.2 scfm⁽⁵⁾* 1.0 cfm 0, 0.83 scfm 0.4

14.0 in. H₂O across blower

24 to 30 Vdc (28 Vdc nominal)

115 W (max.) (109.2 W nominal) 14 A @ 28 Vdc for 1.0 msec

5 A @ 28 Vdc

Cabin ambient (5 psia nominal)

58° to 90°F 58° to 90°F

0° to 140°F

250 hr

613 gm

11.4 cfm

2 in. H₂0

Cabin ambient (5 psia nominal)

10 units (5 with motors) (5 without motors)

0 to 45 ml/sec 5 ml/sec (nominal)

1 cfm[©], 1.03 to 1.195 cfm[©] (seated)**, 1.145 to 1.150 cfm[®] (unseated)**

Cabin ambient

37.3 psid 52.0 psid

*Drawers 1, 2, and 3 tested at 28 Vdc, 14.7 psia, and 70°F. **Drawers 1, 2, and 3 tested at 28 Vdc and c=0.0271 lb/ft3.

S - SPECIFICATION

T = TEST

Amendment 81 (05/11/73) ::SC-01549 (Vol. IV) Rev A

(Urine inlet closed) 12.2 in. H₂0 (min.) With Astronaut Seated on Fecal Collector (Urine inlet closed) With Astronaut Sested 1.9 in. H₂0 (min.) (Urine inlet open) Temperature Range Urine Inlet 98.6°F Gas Inlet 58° to 90°F Separator Capacity Range (Micturition input) 35 to 600 ml Nominal 350 m1* Quantity of Gas in Discharged 1%/day (max.) Liquid Quantity of Liquid in Discharged 0.0 Gas Leakage Rate Gas 1.4 sccs (max.) Liquid None Electrical 24 to 30 Vdc (28 Vdc nominal) Voltage Power Nominal 28 W Locked Rotor 3 A @ 28 Vdc Overload Protection (Circuit 3 A breaker) Motor Speed @ 28 Vdc 15,000 rpm Drum Speed (Dry) @ 24 Vdc (Drawers 1,2, and 3) 205, 198, 184 rpm @ 26 Vdc (Drawers 1,2, and 3) 228, 218, 208 rpm @ 28 Vdc (Drawers 1,2, and 3) 250, 239, 229 rpm @ 30 Vdc (Drawers 1,2, and 3) 271, 258, 250 rpm Time Delay Between Uses 5 min (min.) 4 min 59 sec to 5 min 19 sec Time Period Between Blower Motor Off and Separator Motor Off

Filter Rating (Separator)

Chiller Assembly

Refrigerant Loop Flow Characteristics Urine Sample Chilled Temperature

Urine Pool Chilldown Time to 59°F

Characteristics

Urine Inlet to Plenum Differential (Blower running) With Astronaut Standing

Bladder Assembly (1889060)

Volume

Bladder Internal Pressure (Pressure plate)

Umbrella Valve Cracking Pressure (Urine inlet) See Paragraph 3.1.2.6

Values

14.0 in. H₂0 (min.)

41° to 59°F 2 hr (max.)

10 to 20 ½

4000 ml (min.)

0.5 to 4.0 in. H₂0

0.5 in. H₂0

*Filling above 700 ml results in degraded flow.

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Characteristics	Values				
Temperature Range					
Nonoperating Operational	-40° to 160°F 58° to 90°F				
Leakage (Max.)					
Shutoff Valve (Bladder pressurized with GN ₂ to aP of 12 ±2 in. H ₂ 0)	None detectable H_2^0 ΔP of GN_2	at 12 ±2 in.			
Umbrella Check Valve	None detectable AP of GN ₂	at 12 <u>+</u> 2 in. H ₂ (
Collection Capability	<u>Fecal</u>	Urine			
Maximum Collection Capability (Using blower motor)	300 g (feces) 500 ml (diarrhea)	4000 ml			
Maximum Initial Preparation Duration	30 sec	30 sec			
Maximum buration of Each Complete Cycle (Including preparation and initiation of processing but ex- cluding elimination)	8 min	l min			
Normal Collection Unit Usage					
Cycles/Day/Man Daily Duration (3 crewmen)	1 45 min	10 max. 150 min			
Operational Life	1400 cycles	7000 cycles			
Maximum Time for Removal and Replacement of 3 Urine Col- lection and Sample Bags and Preparation for Freezing		20 min			
24-hr Urine Pooling Volume Measure- ment Accuracy		, ,			
Mechanical Method (On-orbit) Lithium Chloride (LiCl) Method (on ground after sample return)	±15% ±2%	··			

MCDONNELL X

Characteristics	Values
Processor (1879136)	
· Processing Chambers (Drawers)	6
Processing Chamber Volume	304 in ³
Processing Operating Temperature (Controlled via heater controller/sensor)	105 ±5°F ⁶ , 109.6°, 106.9°, 104.8°, 108.8°, 106.2°, 105.4°F (Drawers 1 through 6, respectively, @ 28 Vdc) [©]
Input Voltage Range	24 to 30 Vdc (28 Vdc nominal)
Power Rating	
Heater (Drawers 1 through 6)	93.5 W @ 28 ⁺² Vdc 81.2 to 81.8 W
Heiter Controller/Sensor	2.5 ₩ @ 28 Vdc [©]
Timer	2.1 W
Timer Delay Relay	·
During First 15-min Processor Operation	1.0 W
After 15-min Processor Operation	0.4 W
Overload Protection (Circuit breaker)	5.0 A
Vacuum Line Flow Rate	400 gm/hr @ 0.015 psid and 50° to 105°F
Over-Temperature Control Circuit	•
Opens	165 <u>+</u> 5°F*
Closes	145 <u>+</u> 5°F
Timer Range (Manually adjustable and set as a function of sample weight, automatic shutoff at end of selected drying cycle)	0 to 20 hr
Temperature Range	
Operational	58° to 90°F
Nonoperating	-40° to 160°F
Operational Life	280 heating cycles/processor
Processed Waste Volume/Dump	0.176 ft ³
Waste Processor Exhaust Pressure (Vacuum vent valve open)	0.0005 to 0.06 psia
Vent Screen Mesh Opening	0.062 in.

 \star The heater and timer stops, showing required drying time remaining.

- S = SPECIFICATION
 T = TEST

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	•
<u>Cha:acteristics</u>	<u>Values</u>
Processor Control Valve (1B78648)	l per processor
Flow Rate	2.0 in. H ₂ O ΔP @ 5.5 scfm chamber to vacuum flow
Nominal Pressure Range	0 to 6 psid
Proof	$_{-0}^{+2}$ psid
Burst	65 psid
Temperature Range	
Nonoperating Operational Flow Media	45° to 90°F 45° to 105°F 55° to 105°F
Handle Torque (Manual)	20 in 1b (max.)
Leakage	
Internal at $6 \begin{array}{c} +2 \\ -0 \end{array}$ psid GN_2	<0.6 scim
External at $6 \begin{array}{c} +2 \\ -0 \end{array}$ psid GN_2	<0.1 scim
Pressure Indicator Range	U to U.2 psia

G,

SKYLAB SYSTEM/OPERATIONS ASSESSMENT REVIEW WASTE PROCESSOR

SA -3462-3 4-26-72

FECAL PROCESSOR POWER REQUIREMENTS

- 3 DEFECATIONS / DAY TOTAL
- 200 GM/DEFECATION AVERAGE
- 300 GM/DEFECATION MAXIMUM
- 8.5 HOURS REQUIRED TO PROCESS 200 GM AT 1050 HEATER TEMPERATURE
- 10.5 HOURS REQUIRED TO PROCESS 300 GM AT 1050 F HEATER TEMPERATURE
- 86 WATTS PEAK POWER PER PROCESSOR
- 35 WATTS AVERAGE POWER PER PROCESSOR DURING OPERATION

MICHONNELL DUUGLAS ASTHONAUTICS COMPANY

SKYLAB SYSTEM/OPERATIONS ASSESSMENT REVIEW PROCESSING POWER REQUIREMENTS

SA -3464 4-26-72

DIARRHEA PROCESSING POWER REQUIREMENTS (CONTINGENCY)

- THREE DIARRHEA DEFECATIONS/WEEK
- 1000 CC/WEEK
- 200 CC/DEFECATION MINIMUM
- 300 CC/DEFECATION AVERAGE
- 500 CC/DEFECATION MAXIMUM
- 13.7 HOURS REQUIRED TO PROCESS 200 CC AT 1050 HEATER TEMPERATURE
- 18.2 HOURS REQUIRED TO PROCESS 300 CC AT 1050F HEATER TEMPERATURE
- 31.2 HOURS REQUIRED TO PROCESS 500 CC AT 1050 HEATER TEMPERATURE
- 86 WATTS PEAK POWER PER PROCESSOR
- 30 WATTS AVERAGE POWER PER PROCESSOR DURING OPERATION

MCDONNELL DOUGLAS ASTRONAUTICS COMPANY

SKYLAB SYSTEM/OPERATIONS ASSESSMENT REVIEW PROCESSING POWER REQUIREMENTS

SA-3464-1 4-26-72

VOMITUS PROCESSING POWER REQUIREMENTS (CONTINGENCY)

3 VOMITUS COLLECTIONS PER WEEK

1000 CC/WK

200 CC MINIMUM

300 CC NOMINAL

500 CC MAXIMUM

- 8. 1 HOURS REQUIRED TO PROCESS 200 CC AT 1050 HEATER TEMPERATURE
- 11.7 HOURS REQUIRED TO PROCESS 300 CC AT 1050 HEATER TEMPERATURE
- 27.0 HOURS REQUIRED TO PROCESS 500 CC AT 1050 HEATER TEMPERATURE
- 86 WATTS PEAK POWER PER PROCESSOR
- 35 WATTS AVERAGE POWER PER PROCESSOR DURING OPERATION

SKYLAB

- Fecal and Urine Collection Expendable Items Usage Summary

	Quantity	First manned period		Second manned period			Third manned period					
I ten	onboard at launch	Expected usage			Expected usage	Actual usage	Total remaining				· Remarks	
Fecal bags Contingency	465 185	84	48 1	417 184	168	135 7	· 282 177	168	192 0	90 177	*A; required	
fecal bags Urine collection bags	432	84	75	360	168	178	185	168	185	0	Includes 3 bags carried by the first and second crews	
Urine sample bags	375	66	63	312	132	108	204	132	204	0		
Une-half urine sample bags	125	18	21	104	36	71	33	36	53	0	Includes 20 bags carried by the third crew	
MISSION DURATION			28 DA	.YS	59	DAYS		8	DAY!	5		



MCDONNELL DOUGLAS CORPORATION

APPENDIX D
SYSTEM REQUIREMENTS
DEFINITION DOCUMENT
(CONTAINED IN OTHER BOOKLET)

APPENDIX E

LAYOUTS OF WCS DESIGN CONCEPTS